## Appendix I <br> Traffic Technical Memorandum

# Transportation Technical Memorandum Nelson Sloan Quarry Restoration Project, San Diego 

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### 1.1 Purpose and Scope

The purpose of this memorandum is to analyze the traffic effects associated with the proposed Nelson Sloan Quarry Restoration Project (proposed project) located in the Tijuana River Valley Community in the City of San Diego. The project site is located on approximately 40 acres owned by the County of San Diego. The lead agency for the project is the California Department of Parks and Recreation (CDPR). As the lead agency, CDPR is proposing the beneficial re-use of excess sediment excavated from on-going and proposed sediment management activities in the Tijuana River Valley towards landform and habitat restoration on the abandoned Nelson Sloan Quarry site. This would allow the excess sediment that is currently hauled to offsite to regional landfills or construction sites from the City, County, State and Federal entities (hereby referred as sediment management sites) in Tijuana River Valley (TRV) to be placed in the Nelson Sloan Quarry site as an option. The proposed project would allow these entities to place appropriate material on the quarry site and thereby improve TRV land managers ability to conserve and restore high-quality habitat impacted by sedimentation, and better protect valley-wide infrastructure from sedimentation and flooding.

This memorandum evaluates the proposed project's effects related to the traffic generated by workers and trucks that would be required for the above-mentioned project activities. The objectives of this memorandum are:

- Document existing traffic conditions in the study area;
- Describe active transportation and transit facilities in the vicinity of the project site;
- Estimate trip generation, distribution, and assignment characteristics for the average operational phase of the proposed project (for purposes of this memorandum, "operational" refers to the 10 to 15-year timeframe of reclamation and restoration activities on the proposed project site);
- Provide a Vehicle Miles Traveled (VMT) screening analysis per Senate Bill (SB) 743 requirements under California Environmental Quality Act (CEQA);
- Analyze the traffic effects that would occur under the Opening Year without and with Project conditions; and,
- If required, identify improvement and traffic control measures for effected study area intersections.

This memorandum has been prepared per the County of San Diego Transportation Study Guidelines, May 2020 (Draft), and the City of San Diego Transportation Study Manual, June 2020 (Draft) requirements, and is consistent with the current requirements of all applicable City and State regulations, including SB 743 requirements CEQA.

Dudek analyzed the selected study area intersections for the following study scenarios:

## Existing Condition

The memorandum includes a description of existing traffic conditions in the site vicinity, including the existing roadway system, existing weekday AM and PM peak hour traffic volumes, and traffic operations. The existing condition is representative of the year 2020 (it should be noted that the traffic counts were collected in January, 2020 before COVID-19 restrictions were in effect). However, it was noted that there was nominal truck traffic observed during this period due to seasonal nature of sediment removal activities (generally between August November). Therefore, worker and truck traffic from the sediment management sites was estimated (using best available data from truck activity logs and other reports) and added to the opening year conditions described below.

## Opening Year no Project Condition

The Opening Year condition includes traffic volumes and operations within a short-term horizon period where the proposed project would be operational. An ambient annual growth factor of one percent (1\%) generally based on the San Diego Association of Governments (SANDAG) traffic volume forecasts in the study was applied to the existing year (2020) traffic volumes over the course of two years to estimate opening year baseline traffic volumes in the year 2022.

Along with ambient growth, traffic generated by other approved and pending projects along with the traffic from the existing sediment management sites in the study area was also added to existing traffic volumes. The approved or pending projects are developments in the review process, but not fully approved; or, projects that have been approved, but not fully constructed or occupied. Worker and truck traffic from the sites involving on-going sediment removal activities near the proposed project was added to the opening year traffic conditions.

## Opening Year plus Project Condition

This condition includes analysis of traffic operations under the Opening Year condition (described above) with project traffic added to the AM and PM peak hour traffic volumes. It should be noted that under the Opening Year plus Project conditions a majority of truck traffic from the above-mentioned sediment management sites would travel to the proposed project instead of traveling to other construction sites or landfills in the San Diego County. Therefore, the proposed project would generate nominal new truck trips and divert most of the existing truck trips from the sediment management sites to the project site. The project effects to the roadway network under this condition were used as the basis for determining if any traffic improvements or control plan would be required.

### 1.2 Project Description, Location and Study Area

The project site is located within the southeastern corner of Tijuana River Valley Regional Park in the in the City of San Diego. It is located west of Interstate (I) 5. Regional access to the project is provided by I-5, I-805 and State Route 905 . Local access to the proposed project would be primarily via Dairy Mart Road which turns into Monument Road, at the Dairy Mart Road/Monument Road intersection. Figure 1 shows the project location and site, study area, and regional location of the project site. Figure 1 also illustrates the locations of the sediment management sites in the vicinity of the project site.

The proposed project operations would include placement of processed sediment excavated from management sites as part of on-going annual channel and basin maintenance activities in the Tijuana River Valley. Under existing conditions, most of the sediment excavated from management sites is hauled out of the valley. With the implementation of the proposed project, this sediment would be re-used towards the restoration of the quarry and construction of natural landforms on the quarry site. Therefore, the proposed project would reduce the need to haul sediment from in-valley sites to landfill or construction sites located outside of the TRV in the County.

Based on review of historic data of sediment removal activities, maximum export (in cubic yards) of material anticipated for each sediment management site and required haul truck trips, capacity of haul trucks (in cubic yards) and the project's operational phasing and schedule, and as shown in Section 2 Project Traffic and VMT Screening Analysis, it is anticipated that a daily average of 14 workers, 3 vendor trucks and 6 haul trucks would be required over the life of the project. The project related activities will occur approximately between 6:00 am and 6:00 pm over the weekdays, Monday through Friday.

Based on the location of the project site and transportation network that provides regional and local access to it, study area for assessing the traffic effects of the proposed project was delineated. As illustrated in Figure 1, the study area is comprised of the following nine (9) intersections:

## Intersections

1. Interstate 5 (I-5) northbound ramps/San Ysidro Boulevard (Caltrans)
2. Dairy Mart Road/San Ysidro Boulevard (City of San Diego)
3. Dairy Mart Road/l-5 southbound ramps (Caltrans)
4. Dairy Mart Road/Servando Avenue (City of San Diego)
5. Dairy Mart Road/Camino De La Plaza (City of San Diego)
6. Clearwater Way/Dairy Mart Road (City of San Diego)
7. Monument Road/Dairy Mart Road (City of San Diego)
8. Hollister Street/Monument Road (City of San Diego)
9. Hollister Street/Tocayo Avenue (City of San Diego)

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### 1.3 Analysis Methodology

### 1.3.1 Vehicle Miles Traveled (VMT) Analysis for CEQA

The Governor's Office of Planning and Research (OPR) approved the addition of new Section 15064.3, "Determining the Significance of Transportation Impacts" to the State's CEQA Guidelines, compliance with which is required beginning July 1, 2020. The Updated CEQA Guidelines state that "generally, vehicle miles traveled (VMT) is the most appropriate measure of transportation impacts" and define VMT as "the amount and distance of automobile travel attributable to a project." It should be noted that "automobile" refers to on-road passenger vehicles, specifically cars and light trucks. OPR has clarified in the Technical Advisory and recent informational presentations that heavyduty truck VMT is not required to be included in the estimation of a project's VMT. Other relevant considerations may include the effects of the project on transit and non-motorized traveled.

The new Section 15064.3(b), "Criteria for Analyzing Transportation Impacts," states "If existing models or methods are not available to estimate the vehicle miles traveled for the particular project being considered, a lead agency may analyze the project's vehicle miles traveled qualitatively. Such a qualitative analysis would evaluate factors such as the availability of transit, proximity to other destinations, etc. For many projects, a qualitative analysis of construction traffic may be appropriate."

To aid in this transition, OPR released a Technical Advisory on Evaluating Transportation Impacts in CEQA (December of 2018) (Technical Advisory). Based on the technical Advisory, the City of San Diego and County of San Diego have adopted VMT specific guidelines and thresholds. However, since CDPR is the lead agency, the guidance provided by the State has also been used to determine if the proposed project would require a VMT analysis. The details of applicable VMT screening and analysis has been provided in Chapter 3 of this memorandum.

### 1.3.2 Level of Service (LOS) for General Plan Consistency

Level of Service (LOS) is a tool used to describe the operating characteristics of the street system in terms of the level of congestion or delay experienced by vehicles with service levels range from $A$ through $F$.

### 1.3.2.1 Intersection Analysis

The Highway Capacity Manual, 6th Edition (HCM 6) methodology was used to assess level of service for intersections within the study area per requirement of the respective jurisdiction.

The HCM intersection analysis methodology was used to analyze the operation of signalized and unsignalized study intersections. The HCM method used to determine LOS at the intersections determines the average control delay (in seconds) a driver may experience at the intersection. The HCM analysis methodology describes the operation of an intersection using a range of LOS from LOS A (free-flow conditions) to LOS F (severely congested conditions), based on the corresponding control delay experienced per vehicle for unsignalized intersections. The Synchro 10 LOS software was used to determine intersection LOS. Synchro is consistent with the HCM 6 methodology (Transportation Research Board 2016). Table 1 shows the LOS values by delay ranges for unsignalized and signalized intersections under the HCM methodology.

## Table 1. Levels of Service for Intersections using HCM Methodology

| Level of Service | Unsignalized Intersections <br> Control Delay (in seconds per vehicle) | Signalized Intersections <br> Control Delay (in seconds per vehicle) |
| :---: | :--- | :--- |
| A | $<10.0$ | $<10.0$ |
| B | $>10.0$ to $<15.0$ | $>10.0$ to $<20.0$ |
| C | $>15.0$ to $<25.0$ | $>20.0$ to $<35.0$ |
| D | $>25.0$ to $<35.0$ | $>35.0$ to $<55.0$ |
| E | $>35.0$ to $<50.0$ | $>55.0$ to $<80.0$ |
| F | $>50.0$ | $>80.0$ |

Source: HCM 6
Additionally, the following parameters were used in the operational analysis for the intersections per requirements specified in the City of San Diego TSM:

- The morning and afternoon peak commute hours were analyzed, for peak hour between 7:00-9:00 p.m. and 4:00-6:00 p.m.
- Peak hour factors (PHF) from traffic counts collected in January 2020 were used in the Existing and Opening Year (with and without project) scenarios.
- Peak hour truck percentages for each turning movement were obtained from the field data collected in January 2020. However, since the truck traffic in the study area is seasonal and was not accounted for in the counts conducted in January 2020, the minimum recommended value of $3 \%$ was applied to Existing and Opening Year (with and without project) conditions.
- Existing non-PCE peak hour traffic volumes were analyzed using HCM methodology. These volumes were adjusted to include a "heavy vehicle percentage" within Synchro. Use of the heavy vehicle percentage factor within Synchro more accurately estimates the operation of an intersection that is being evaluated with the HCM methodology. However, the truck traffic from the project and other sites was converted into PCE volumes and added to the existing non-PCE traffic volumes to obtain Opening Year (with and without project) traffic volumes.
- Signal timing and cycle length data was obtained from field data collected in January 2020.


### 1.3.2.2 General Plan Consistency Requirements

The following section provides the consistency requirements for the City of San Diego and County of San Diego that would apply to the proposed project.

## City of San Diego General Plan Mobility Element

The level of service guideline is established in the City of San Diego General Plan Mobility Element (June 2015). According to Mobility Element Policy for Project Review Considerations:
"ME-C.9. Implement best practices for multi-modal quality/level of service analysis guidelines to evaluate potential transportation improvements from a multi-modal perspective in order to determine optimal improvements that balance the needs of all users of the right of way."

The City has not adopted a specific LOS standard and performance of signalized and unsignalized intersections is evaluated on a case-by-case basis.

## County of San Diego General Plan Mobility Element

The level of service guideline is established in the County of San Diego General Plan Mobility Element (August 2011). According to Circulation Element Policy for Project Review Considerations:
"Goal M2 - Responding to Physical Constraints and Preservation Goals. Level of Service Criteria. Require development projects to provide associated road improvements necessary to achieve a level of service of "D" or higher on all Mobility Element roads except for those where a failing level of service has been accepted by the County."

### 1.4 Improvements for Transportation Impacts

### 1.4.1 VMT Impacts

To mitigate VMT impacts, the project applicant would be required to reduce VMT, which can be done by either reducing the number of automobile trips generated by the project or by reducing the distance that people drive. The following strategies are available to achieve this:

- Modify the project's site design and built physical characteristics to reduce VMT generated by the project.
- Implement programmatic Transportation Demand Management (TDM) measures to reduce VMT generated by the project.


### 1.4.2 Level of Service Inconsistency

The City of San Diego requires that off-site improvements should address access, circulation and safety for all modes in order to accommodate project traffic. Improvements to signalized and unsignalized intersections should be based on conflicting pedestrian movements, existing and proposed bicycle facilities, transit priority, protected or permissive turn movement phasing, number of lanes, speed of prevailing traffic and expected queue lengths.

The County of San Diego requires traffic operational impacts and improvements should be identified based on the triggers specified in the guidelines in the Local Mobility Analysis for signalized intersections and unsignalized intersections.

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# 2 <br> Project Traffic and VMT Screening Analysis 

This section documents the trip generation, distribution, and assignment of project traffic. The section also provides a Vehicles Miles Traveled (VMT) screening analysis based on the proposed project's trip generation using the State, County and City of San Diego's recently adopted CEQA transportation guidelines.

### 2.1 Trip Generation

The Institute of Transportation Engineers' Trip Generation manual does not contain trip rates for quarry-related activities. Project-related traffic includes the number of workers, and the amount of vendor and haul truck traffic that would be generated to and from the site's daily and during the AM and PM peak hours. The operational activities of the site for quarry reclamation, landform creation and habitat restoration include sediment placement, grading, and revegetation. Therefore, the proposed project's operational phasing and schedule used in the Air Quality analysis was obtained. This phasing and schedule included worker and truck trips for each phase of the proposed project over a 15-year period and included the number of workers, vendor trucks (material and equipment delivery) and haul trucks (soil export/sediment management) that would be required for the proposed project's operational activities. As shown in Table 2, a daily average of 14 workers, 3 vendor trucks and 72 haul trucks would be required for most phases of the project-related activities.

As mentioned previously, the proposed project would allow include placement of processed sediment excavated from management sites as part of on-going annual channel and basin maintenance activities in the Tijuana River Valley. Therefore, the sediment excavated from management sites that is hauled out of the valley under existing conditions would be re-used towards the restoration of the quarry and creation of natural landforms on the quarry site. Therefore, the proposed project would reduce the need to haul sediment from in-valley locations to other landfill or construction sites located outside of the TRV in the County of San Diego. To estimate this reduction in truck trips, worker and truck traffic from the sediment management sites was estimated using available data sources. These included truck haul logs provided by Goat Canyon Sediment Basin administrators (CDPR) and maximum export data (in cubic yards) for other sites (included in Table 2 and shown on Figure 1) provided in the City of San Diego Municipal Waterways and Maintenance Plan (MWMP) Final EIR (City of San Diego 2020). Based on review of available data for these sites, an estimate of workers and trucks was prepared and is shown in Table 2.

Table 2. Worker and Truck Estimates for Sediment Management Sites and Proposed Project

| Site | No. of Workers | Daily Vendor Trucks | Total Haul Trucks |
| :---: | :---: | :---: | :---: |
| Sediment Management Sites |  |  |  |
| Goat Canyon Sediment Basin | 15 | 5 | 32 |
| Smuggler's Gulch Emergency and Pilot Channel (City of San Diego) | 12 | 5 | 25 |
| Smuggler's Gulch (County of San Diego) | 2 | 1 | 4 |
| United States International Boundary and Water Commission (USIBWC) | 5 | 1 | 5 |
| Sub-total | 34 | 12 | 66 |

# Table 2. Worker and Truck Estimates for Sediment Management Sites and Proposed Project 

| Site | No. of <br> Workers | Daily Vendor <br> Trucks | Total Haul <br> Trucks |
| :--- | :--- | :--- | :--- |
| Proposed Project | 14 | 3 | $6^{1}$ |
| Nelson Sloan Quarry Restoration |  |  |  |

## Notes:

1 The daily net haul trucks $(72-66=6)$ were estimated by subtracting the haul trucks generated by existing sediment management activities from haul trucks that would be generated by the proposed project.

As shown in Table 2, a daily average of approximately 34 workers, 12 vendor trucks and 66 haul trucks would be generated to and from the sediment management sites. The approximately 66 haul trucks from these sites would travel to the proposed project site once operational. Therefore, the net new haul truck traffic estimated for the proposed project would reduce to 6 haul trucks from estimated 72 trucks that are required for the operational phases.

As estimated, a daily average of 14 workers, 3 vendor trucks and 6 net new haul trucks would be required for most phases of the project-related activities. The project-related activities will occur between 6:00 am and 6:00 pm over the weekdays, Monday through Friday. Based on the work schedule, some of the workers would not travel during the AM or the PM peak periods. However, in order to provide a conservative analysis, all workers (i.e., 14 workers) were assumed to arrive during the AM peak hour and leave the site during the PM peak hour. All truck trips were average over the 8 -hour workday to estimate peak hour trips with $100 \%$ inbound during the AM peak hour and $100 \%$ outbound during the PM peak hour. Passenger car equivalent (PCE) factors were used to account for the project's truck traffic and provide a more realistic measurement in terms of the impact of project-related truck traffic. All vendor truck trips were converted to PCE trips using a factor of 2.5 and all haul truck trips were converted to PCE trips using a factor of 3.0. The calculation of project trip generation estimates is shown in Table 3.

## Table 3. Project Trip Generation

| Vehicle Type | Daily Quantity | Daily Trips | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out | Total | In | Out | Total |
| Trip Generation |  |  |  |  |  |  |  |  |
| Workers | 14 workers | 28 | 14 | 0 | 14 | 0 | 14 | 14 |
| Vendor Trucks | 3 Trucks | 6 | 1 | 0 | 1 | 0 | 1 | 1 |
| Haul Trucks | 6 Trucks | 12 | 2 | 0 | 2 | 0 | 2 | 2 |
|  | Total Trips | 46 | 17 | 0 | 17 | 0 | 17 | 17 |
| Existing On-Site Haul Trucks | 66 Trucks | 132 | 17 | 0 | 17 | 0 | 17 | 17 |
| Trip Generation w/PCE |  |  |  |  |  |  |  |  |
| Workers (1.0 PCE) ${ }^{1}$ | 14 workers | 28 | 14 | 0 | 14 | 0 | 14 | 14 |
| Vendor Trucks (2.5 PCE) ${ }^{2}$ | 3 Trucks | 15 | 3 | 0 | 3 | 0 | 3 | 3 |
| Haul Trucks (3.0 PCE) ${ }^{3}$ | 6 Trucks | 36 | 6 | 0 | 6 | 0 | 6 | 6 |
| Total Trips (w/PCE) |  | 79 | 23 | 0 | 23 | 0 | 23 | 23 |
| Existing On-Site Haul Trucks (3.0 PCE) ${ }^{3}$ | 66 Trucks | 396 | 51 | 0 | 51 | 0 | 51 | 51 |

[^0]1 PCE factor of 1 was utilized for worker passenger cars
2 PCE factor of 2.5 was utilized for vendor trucks
3 PCE factor of 3.0 was utilized for haul trucks

As shown in the Table 3, the proposed project would generate 46 daily trips, 17 AM peak hour trips ( 17 inbound and 0 outbound), and 17 trips during the PM peak hour ( 0 inbound and 17 outbound). With the application of PCE factors to truck trips, the project would generate 79 total PCE daily trips, and 23 PCE trips during the AM peak hour ( 23 inbound and 0 outbound) and 23 PCE trips during the PM peak hour ( 0 inbound and 23 outbound).

### 2.2 Trip Distribution and Assignment

Project trip distribution percentages were based on logical travel paths to commute corridors in the study area as well as analysis of haul truck data provided by CDPR for one of the existing sites (i.e., Goat Canyon Sediment Basin).

Construction-related truck traffic will access the study area via $1-5$, at its existing ramps at Dairy Mart Road and use Dairy Mart Road and Monument Road to access the project site via the existing driveway along Monument Road.

Project trips were assigned to the study area intersections by applying the project trip generation estimates to the trip distribution percentages at each study area intersection.

- The project trip distribution and trip assignment for workers is shown in Figure 2.
- The project trip distribution and trip assignment for off-site trucks is shown in Figure 3.

The project trip distribution and trip assignment for on-site trucks that primarily travel to and from other sediment management sites is shown in Figure 4.

The total project trip assignment for worker and trucks (on-site and off-site) is shown in Figure 5.

## $2.3 \quad$ Vehicle Miles Traveled Screening

OPR has approved the addition of new Section 15064.3, "Determining the Significance of Transportation Impacts" to the state's CEQA Guidelines, compliance with which is required beginning July 1, 2020. The Updated CEQA Guidelines state that "generally, vehicle miles traveled (VMT) is the most appropriate measure of transportation impacts" and define VMT as "the amount and distance of automobile travel attributable to a project." Per OPR, heavy vehicle traffic is not required to be included in the estimation of a project's VMT.

The OPR's Technical Advisory suggests that agencies may screen out VMT impacts using project size, maps, transit availability, and provision of affordable housing. The guidance recommended by OPR has been adopted and modified by the County of San Diego in the Transportation Study Guidelines, May 2020 (Draft) and the City of San Diego in the Transportation Study Manual, June 2020 (Draft) guidelines for VMT requirements to be better suited to local conditions.

The determination of minimum project size for VMT analysis is described below in Table 6 for State, County and City. The level of VMT analysis in Table 4 is recommended based on project size (expressed in terms of Average Daily Trips generated by the project). It should be noted that the State and County recommend that any project generating 110 or less average daily trips may be presumed to have a less than significant impact absent substantial evidence to the contrary. The City of San Diego recommends that any project generating 300 or less average daily trips may be presumed to have a less than significant impact and therefore be screening from a detailed VMT analysis.

Based on the small project screening criteria used by State, County and the City, since the project would generate 79 average daily trips, it can be presumed to have a less than significant VMT impact.

Table 4. VMT Screening for Project

| State Guidance | County of San Diego | City of San Diego |
| :--- | :--- | :--- |
| Small Project - projects that generate | Small Employment Project - Less |  |
| or attract fewer than 110 trips per day |  |  |
| than 110 daily vehicle trips (trips are |  |  |
| generally may be assumed to cause a |  |  |
| less-than significant transportation |  |  |
| impact. | Small Project - The project is a <br> after any alternativer of vehicle trips <br> small project defined as <br> generating |  |
| gened adjustments are applied) |  |  |
| unadjusted drivewan 300 daily |  |  |
| the City of San Diego trip using |  |  |
| generation rates/procedures. |  |  |



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This section describes existing conditions within the study area. Characteristics are provided for the existing roadway system, daily roadway segment traffic volumes, peak hour traffic volumes, and traffic operations.

### 3.1 Roadway System

Characteristics of the existing street system in the study are described below. Figure 6 shows the traffic control and geometrics for intersections in the study area.

Interstate (I-) 5 is a north-south, generally eight-lane, divided freeway located northeast of the project site. The posted speed limit is 65 mph . Within California, $l-5$ connects San Diego, Los Angeles, Sacramento, and the eastern portion of the San Francisco Bay Area. I-5 has a local interchange at Dairy Mart Road/ San Ysidro Boulevard.

State Route (SR-) 905 serves as a major east-west connection between I-5 and the Otay Mesa community. SR-905 has an interchange with I-5 that can be accessed from Tocayo Avenue.

Dairy Mart Road is classified as a Collector in the Tijuana River Valley Community Circulation Plan. It is constructed as a four-lane roadway that runs in the north-south direction from Beyer Boulevard to Camino de la Plaza. South of Camino de la Plaza, the roadway is two lane and between West San Ysidro Boulevard and Camino de la Plaza is not yet built to its ultimate classification. This road provides access to the Tijuana River Valley. Sidewalks are provided along both sides of the roadway between Beyer Boulevard and West San Ysidro Boulevard. Parking is not provided along the entire roadway segment. The posted speed limit between the l-5 interchange and Camino de la Plaza is 40 mph . Dairy Mart Road has a Class II bicycle lane between Beyer Boulevard and West San Ysidro Boulevard.

Monument Road is an east-west two-lane roadway classified as a Collector in the Tijuana River Valley Community Circulation Plan. Dairy Mart Road becomes Monument Road, approximately where the Ranger Station is located just west of the Dairy Mart Road/Monument Road intersection. Monument Road provides an east-west access through Tijuana River Valley. Monument Road is also the main access road utilized by the U.S. Border Patrol. The two-lane roadway is not constructed with sidewalk, curb or gutter and the posted speed limit is $30-35 \mathrm{mph}$.

Hollister Road is a north-south two-lane roadway classified as a Collector in the Tijuana River Valley Community Circulation Plan. The roadway segment of Hollister Road from Tocayo Avenue to Honestidad Road, the two-lane roadway has a painted median. The roadway is built with paved sidewalk, curb and gutter. There is a Class 2 bike lane and the posted speed limit is 30 mph . The roadway segment of Hollister Road from just north of Sunset Avenue to Monument Road is built as a two-lane roadway and is not constructed with sidewalk, curb or gutter. The posted speed limit is 30 mph .

Other roadways in the area include Saturn Boulevard and Sunset Avenue. Saturn Boulevard is a disjointed road that traverses north-south from Monument Road, then east-west from Hollister Street connecting to Sunset Avenue. Sunset Avenue provides an east-west connection through the Tijuana River Valley and is approximately 1.8 miles long.

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### 3.2 Transit, Bicycle and Pedestrian Facilities

Existing bicycle and transit facilities are shown on Figure 7. Existing bicycle and pedestrian volumes counts obtained at the study area intersections are provided in Appendix A.

### 3.2.1 Transit Facilities

The Metropolitan Transit System (MTS) provides public transit service within the study area. Bus routes (906 and 907) serve the area with stops along San Ysidro Boulevard and Camino de la Plaza. The nearest bus stop to the project site is located approximately 1.5 miles far along San Ysidro Boulevard, near the Dairy Mart Road/San Ysidro Boulevard intersection. Bus Route 906 and 907 operates between Iris Transit Center - San Ysidro loop via Beyer Boulevard and San Ysidro Boulevard.

The Blue Line of the San Diego Trolley has station at the Iris Transit Center and the Beyer Boulevard Trolley Station. The Beyer Boulevard Transit Station is located approximately 2.5 miles from the proposed project. The South Line portion of the San Diego Arizona Eastern (SD\&AE) Railway provides a rail connection for the region's freight operations between the U.S.-Mexico border at San Ysidro. MTS operates the Trolley Blue Line using the South Line railway for most hours of the day. During nighttime hours, the South Line functions as a freight line and operates on the tracks within the San Ysidro area.

### 3.2.2 Pedestrian Facilities

The proposed project and its immediate vicinity do not serve many active transportation users. There are no sidewalks along Monument Road near the project access. Dairy Mart Road has discontinuous paved sidewalk along one side of the roadway between San Ysidro Boulevard and Monument Road. The proposed project is near Tijuana River Valley Regional Park which consists of a network of formal trails that provide many settings for hiking, biking, riding horses, and other passive recreation. A discontinuous multi-purpose trail exists along Monument Road which is used for recreation purposes.

### 3.2.3 Bicycle Facilities

The City of San Diego is serviced by Class 1 (Bike path), Class 2 (Bike lane) and Class 3 (Bike route) bicycle facilities. There are discontinuous bicycle facilities in the study area. Within the study area, following are the existing bicycle facilities:

- Dairy Mart Road between Beyer Boulevard to Monument Road
- Camino de la Plaza between Dairy Mart Road and San Ysidro Boulevard
- San Ysidro Boulevard from Dairy Mart Road to Camino de la Plaza
- Hollister Avenue from south of Tocayo Avenue to Coronado Avenue
- Tocayo Avenue from Hollister Avenue to Oro Vista Road

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### 3.3 Existing Traffic Volumes

The existing traffic controls and geometrics at the study area intersections are shown in Figure 6. Existing weekday peak hour turn movement counts at the study intersections and average daily traffic (ADT) counts at the roadway segments near project site were conducted in January 2020, during a typical non-holiday week while area schools were in-session. It should be noted that the traffic counts were collected in January 2020 before COVID-19 restrictions were in effect. Peak hour truck percentages for each turning movement were obtained from the field data collected in January 2020. However, since the truck traffic in the study area is seasonal and was not accounted for in the counts conducted, the minimum recommended value of $3 \%$ was applied to Existing and Opening Year (with and without project) conditions.

Raw traffic count worksheets are provided in Appendix A. This analysis focuses on the weekday daily, AM (7:00 a.m. to 9:00 a.m.) and the PM (4:00 p.m. to 6:00 p.m.) peak periods. The peak periods represent the highest volume of traffic for the adjacent street system.

Existing weekday AM and PM peak hour volumes are summarized on Figure 8 and existing ADTs are summarized in Table 5.

## Table 5. Existing Average Daily Traffic

| Roadway Segment | Existing ADT (No. of Vehicles) |
| :--- | :---: |
| Dairy Mart Road between l-5 to Camino De La Plaza | 9,793 |
| Dairy Mart between Camino De La Plaza and Clearwater | 1,011 |
| Dairy Mart between Clearwater and Monument Rd | 702 |
| Monument Road between Hollister and Dairy Mart | 529 |
| Hollister Street between Tocayo and Sunset | 3,453 |
| Hollister Street between Sunset and Monument | 624 |

Notes: ADT - Average Daily Traffic

### 3.4 Intersection Operations

An intersection LOS analysis was prepared for the existing conditions using the HCM methodologies discussed in Section 1.3.2. Table 6 shows the results of the existing conditions LOS analysis. LOS worksheets are provided in Appendix C.

Table 6. Existing Weekday Peak Hour Intersection LOS

| No. | Intersection | Traffic Control | AM Peak |  | PM Peak |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Delay ${ }^{1}$ | LOS ${ }^{2}$ | Delay ${ }^{1}$ | LOS ${ }^{2}$ |
| 1 | I-5 northbound ramps/San Ysidro Boulevard | Signal | 24.9 | C | 16.9 | B |
| 2 | Dairy Mart Road/San Ysidro Boulevard | Signal | 33.1 | C | 26.0 | C |
| 3 | Dairy Mart Road/l-5 southbound ramps | Signal | 27.4 | C | 40.9 | D |
| 4 | Dairy Mart Road/Servando Avenue | AWSC | 16.0 | C | 14.6 | B |
| 5 | Dairy Mart Road/Camino De La Plaza | AWSC | 10.2 | B | 17.0 | C |

## Table 6. Existing Weekday Peak Hour Intersection LOS

|  |  |  | AM Peak |  | PM Peak |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| No. | Intersection | Traffic Control | Delay ${ }^{1}$ | LOS $^{2}$ | Delay $^{1}$ | LOS $^{2}$ |
| 6 | Clearwater Way/Dairy Mart Road |  | 8.8 | A | 8.7 | A |
| 7 | Monument Road/Dairy Mart Road | Stop-Control | 8.6 | A | 8.6 | A |
| 8 | Hollister Street/Monument Road | Stop-Control | 8.6 | A | 8.8 | A |
| 9 | Hollister Street/Tocayo Avenue | Signal | $\mathbf{2 2 5 . 6}$ | F | 56.9 | E |

Notes: AWSC - All-way stop control
1 Delay is measured in seconds per vehicle
2 Level of Service (LOS)

As shown in the table, the following study area intersection is currently operating at LOS E or worse under existing conditions:

- Hollister Street/Tocayo Avenue (LOS F in the AM peak hour and LOS E in the PM peak hour)


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## 4 Opening Year Conditions

This section presents the analysis of opening year traffic conditions that was conducted for the year 2022 when the project would be operational. The Opening Year conditions are based on the addition of traffic from approved and pending projects as well as sediment management sites in the study area, along with application of an ambient growth factor to the existing 2020 traffic volumes.

### 4.1 Cumulative Projects

The cumulative projects are projects that are proposed and in the review process, but not yet fully approved; or, projects that have been approved, but not fully constructed or occupied. The City of San Diego identified three cumulative projects and the County of San Diego identified one cumulative project that may add traffic to the project study area.

Additionally, the existing sediment management sites that were included in the Opening Year conditions are listed below.

- Goat Canyon Sediment Basin
- Smuggler's Gulch Emergency and Pilot Channel, City of San Diego
- Smuggler's Gulch County of San Diego
- United States International Boundary and Water Commission

Adequate data to estimate worker and truck trip generation for the Tijuana River Valley (Brown Fill) and Tijuana Estuary Tidal Restoration Project (TETRP) (Phase II) projects was not available at the time of preparation of this memorandum. However, the background growth of $1 \%$ is assumed for the study area is conservative and would account for any additional traffic that these sites would generate.

Figure 9 shows the locations, and Table 7 provides a brief description of the cumulative projects.
Table 7. Description of Cumulative Projects

| No. | Cumulative Project/Application <br> No. | Location | Description |
| :---: | :--- | :--- | :--- |
| 1 | Goat Canyon Sediment Basin | South of Monument Rad, <br> west of Hollister Road | On-going- excavation, sorting and hauling <br> of stockpiled waste |
| 2 | County of San Diego <br> Campground and Nature <br> Education Activity Center | 1942 Monument Road | Construction of a campground and nature <br> activity center within an existing 78-acre <br> vacant site. |
| 3A | Smuggler's Gulch Emergency <br> and Pilot Channel (City of San <br> 3B | Diego) <br> (North of Monument Road) | Excavation in Smuggler's Gulch to prevent <br> future flooding of Monument Road and <br> neighboring property. |
| 4 | Smuggler's Gulch (County of <br> San Diego) | South of Monument Road | Ongoing dredging and excavation of <br> materials. |
| 5 | United States International <br> Boundary and Water <br> Commission (USIBWC) | South of Clearwater Way | On-going - Excavation, sorting, and <br> hauling |

Table 7. Description of Cumulative Projects

| No. | Cumulative Project/Application <br> No. | Location | Description |
| :---: | :--- | :--- | :--- |
| 6 | Vista Lane Villas EOT (Project <br> 458862) | 3481 Vista (SB) Lane | Construction of 38 units on a 2.88-acre <br> site. |
| 7 | Mission Villas EOT (Project <br> 458919) | 3515 Vista (SB) Lane | Construction of 14 residential <br> condominium units on a 1.52-acre site. |
| 8 | Blackshaw Lane EOT (Project <br> 458934) | 549 Blackshaw Lane | Development of 11 residential <br> condominium units on a 0.94-acre site. |
| 9 | San Ysidro Senior Village <br> (Project 569507) | 515 W San Ysidro <br> Boulevard | Development of 51 senior living residential <br> units on a 1.25-acre site. |
| 10 | Residential - Saturn Blvd <br> (Project 566657) | 1695 Saturn Boulevard | Construction of 18 residential single <br> dwelling units on a 3.6-acre site. |

### 4.1.1 Trip Generation

The trip generation for the cumulative projects is shown in Table 8. As shown in the table, cumulative projects are forecast to generate approximately 2,752 daily trips, 277 AM peak hour trips, and 333 PM peak hour trips. Figure 10 shows the cumulative project traffic volumes.

Table 8. Cumulative Projects Trip Generation Summary

|  |  |  | Daily | AM P | k Hour |  | PM P | ak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | Land Use/ Description | Units | Trips | In | Out | Total | In | Out | Total |
| 1 | Goat Canyon Sediment Basin ${ }^{1}$ | Workers/ Trucks | 823 | 116 | 0 | 116 | 0 | 116 | 116 |
| 2 | County of San Diego Campground and Nature Education Activity Center ${ }^{2}$ | Acres | 764 | 15 | 22 | 37 | 52 | 24 | 76 |
| $\begin{gathered} \hline \text { 3A } \\ \& \\ \text { 3B } \end{gathered}$ | Smuggler's Gulch Emergency and Pilot Channel (City of San Diego) ${ }^{1}$ | Workers/ Trucks | 199 | 38 | 0 | 38 | 0 | 38 | 38 |
| 4 | Smuggler's Gulch (County of San Diego) ${ }^{1}$ | Workers/ Trucks | 33 | 8 | 0 | 8 | 0 | 8 | 8 |
| 5 | United States International Boundary and Water Commission (USIBWC) ${ }^{1}$ | Workers/ <br> Trucks | 45 | 14 | 0 | 14 | 0 | 14 | 14 |
| 6 | Vista Lane Villas EOT (Project 458862) ${ }^{2}$ | DU | 304 | 5 | 19 | 24 | 21 | 9 | 30 |
| 7 | $\begin{aligned} & \text { Mission Villas EOT (Project } \\ & 458919)^{2} \\ & \hline \end{aligned}$ | DU | 112 | 2 | 7 | 9 | 8 | 3 | 11 |
| 8 | $\begin{aligned} & \text { Blackshaw Lane EOT (Project } \\ & 458934)^{2} \end{aligned}$ | DU | 88 | 1 | 6 | 7 | 6 | 3 | 9 |
| 9 | San Ysidro Senior Village (Project 569507) ${ }^{2}$ | DU | 204 | 4 | 6 | 10 | 8 | 6 | 14 |
| 10 | $\begin{array}{\|l} \hline \begin{array}{l} \text { Residential - Saturn Blvd (Project } \\ 566657)^{2} \end{array} \\ \hline \end{array}$ | DU | 180 | 4 | 10 | 14 | 13 | 5 | 18 |
| Total Trip Generation |  |  | 2,752 | 206 | 70 | 276 | 108 | 226 | 334 |

Notes: DU = dwelling unit

1 Trip Generation based on worker and truck trip estimate for maximum export of material for the sediment management site.
2 Trip generation based on trip rates from SANDAG 2002

### 4.1.2 Trip Distribution and Assignment

Trip distributions and assignments for the cumulative projects were developed assuming logical commute corridors. The trips generated by the cumulative projects were distributed and assigned through the study area network.

### 4.2 Traffic Volumes

Opening Year traffic volumes include traffic from ambient growth, and traffic from the addition of cumulative projects in the vicinity of the project. A growth rate of $1.0 \%$ per year, based on the SANDAG traffic forecast was applied to the existing traffic volumes to account for the Opening conditions. Figure 11 illustrates the Year 2022 (no project) traffic volumes for peak hour conditions.

### 4.3 Intersection Operations

An intersection LOS analysis was prepared for the Opening Year conditions using the HCM methodology. Table 7 summarizes the results of the Opening Year conditions intersection analysis for the AM and PM peak hours. Detailed LOS calculation worksheets are included in Appendix C.

## Table 9. Opening Year Peak Hour Intersection LOS

| No. | Intersection | Traffic Control | AM Peak |  | PM Peak |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Delay ${ }^{1}$ | LOS $^{2}$ | Delay ${ }^{1}$ | LOS ${ }^{2}$ |
| 1 | I-5 northbound ramps/San Ysidro Boulevard | Signal | 26.9 | C | 17.4 | B |
| 2 | Dairy Mart Road/San Ysidro Boulevard | Signal | 38.7 | D | 47.4 | D |
| 3 | Dairy Mart Road/l-5 southbound ramps | Signal | 30.8 | C | 47.3 | D |
| 4 | Dairy Mart Road/Servando Avenue | AWSC | 18.6 | C | 32.7 | D |
| 5 | Dairy Mart Road/Camino De La Plaza | AWSC | 12.6 | B | 23.0 | C |
| 6 | Clearwater Way/Dairy Mart Road | Stop-Control | 9.6 | A | 9.8 | A |
| 7 | Monument Road/Dairy Mart Road | Stop-Control | 9.1 | A | 9.6 | A |
| 8 | Hollister Street/Monument Road | Stop-Control | 9.5 | A | 10.2 | B |
| 9 | Hollister Street/Tocayo Avenue | Signal | 236.9 | F | 61.9 | E |

[^1]1 Delay is measured in seconds per vehicle
2 Level of Service (LOS)
As shown in the table, the following study area intersection would continue to operate at LOS E or worse under Opening Year conditions:

- Hollister Street/Tocayo Avenue (LOS F in the AM peak hour and LOS E in the PM peak hour)

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## 5 Opening Year Plus Project Conditions

This section describes project impacts under Opening Year plus Project conditions within the study area for intersection operations and analyzes per the City of San Diego and County of San Diego guidelines.

### 5.1 Traffic Volumes

The project trip assignment, as shown in Figure 5, was added to the Opening Year traffic volumes, as shown in Figure 11, to derive the Opening Year plus Project traffic volumes. Figure 12 shows the Opening Year plus project traffic volumes. The existing intersection geometrics in the study area have been assumed to be maintained through the Opening Year plus Project traffic scenario, as shown in Figure 6.

### 5.2 Intersection Operations

An intersection LOS analysis was prepared for the Opening Year plus Project condition using the HCM methodology. Table 10 summarizes the results of the Opening Year plus Project intersection analysis for the AM and PM peak hours. Detailed LOS calculation worksheets are included in Appendix C.

As shown in the table, the following study area intersection would continue to operate at LOS E or worse under Opening Year plus Project conditions:

- Hollister Street/Tocayo Avenue (LOS F in the AM peak hour and LOS E in the PM peak hour)

As shown in the table, the addition of project traffic would contribute to the Hollister Street/Tocayo Avenue intersection that is currently operating at an unacceptable level of service. However, based on the criteria specified by the City of San Diego for signalized intersections, the proposed project would not be required to make any improvements to this intersection.

City of San Diego:

- The project does not add 50 peak hour trips to the Hollister Street/Tocayo Avenue intersection, therefore is not required to be included in the project's study area;
- The project does not add traffic to an individual left turn movement causing the total number of peak hour left turns to exceed 300.
- The project does not add traffic to an individual right turn movement causing the total number of peak hour right turns to exceed 500.

Table 10. Opening Year plus Project Peak Hour Intersection Level of Service

| No | Intersection | LOS Method | Opening Year |  |  |  | Opening Year plus Project |  |  |  | Change in Delay |  | Unacceptable LOS |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM Peak |  | PM Peak |  | AM Peak |  | PM Peak |  |  |  |  |  |
|  |  |  | Delay ${ }^{1}$ | LOS ${ }^{2}$ | Delay ${ }^{1}$ | LOS ${ }^{2}$ | Delay ${ }^{1}$ | LOS ${ }^{2}$ | Delay ${ }^{1}$ | $\mathrm{LOS}^{2}$ | AM | PM | AM | PM |
| 1 | I-5 northbound ramps/San Ysidro Boulevard | Signal | 26.9 | C | 17.4 | B | 26.9 | C | 17.5 | B | 0.00 | 0.10 | No | No |
| 2 | Dairy Mart Road/San Ysidro Boulevard | Signal | 38.7 | D | 47.4 | D | 38.7 | D | 50.1 | D | 0.00 | 2.70 | No | No |
| 3 | Dairy Mart Road/l-5 southbound ramps | Signal | 30.8 | C | 47.3 | D | 31.2 | C | 48.1 | D | 0.40 | 0.80 | No | No |
| 4 | Dairy Mart Road/Servando Avenue | AWSC | 18.6 | C | 32.7 | D | 18.9 | C | 36.5 | E | 0.30 | 3.80 | No | No |
| 5 | Dairy Mart Road/Camino De La Plaza | AWSC | 12.6 | B | 23.0 | C | 13.0 | B | 23.5 | C | 0.40 | 0.50 | No | No |
| 6 | Clearwater Way/Dairy Mart Road | Stop-Control | 9.6 | A | 9.8 | A | 9.7 | A | 9.9 | A | 0.10 | 0.10 | No | No |
| 7 | Monument Road/Dairy Mart Road | Stop-Control | 9.1 | A | 9.6 | A | 9.6 | A | 10.8 | B | 0.50 | 1.20 | No | No |
| 8 | Hollister Street/Monument Road | Stop-Control | 9.5 | A | 10.2 | B | 9.7 | A | 10.7 | B | 0.20 | 0.50 | No | No |
| 9 | Hollister Street/Tocayo Avenue | Signal | 236.9 | F | 61.9 | E | 236.2 | F | 61.8 | E | $-0.70^{3}$ | $-0.10^{3}$ | Yes | Yes |

Notes: AWSC - All way stop control
BOLD value indicates unsatisfactory LOS
1 Volume-to-Capacity (V/C) ratio
2 Level of Service (LOS)
3 Occasionally addition of traffic to a movement reduces the overall average delay (in seconds) of the intersection


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## 6 Project Access Analysis

As mentioned in Section 1, the access to the proposed project would be from Monument Road via the unsignalized intersection of Dairy Mart Road/Monument Road (Intersection 7).

The section of Monument Road west of Dairy Mart Road/Monument Road intersection has a posted speed limit of $30-\mathrm{mph}$. As shown on Figure13, there is adequate sight distance at the Dairy Mart Road/Monument Road intersection looking from theeastbound and westbound direction towards the northbound approach (i.e. the access to the proposed project). Itis recommended that any shrubs/vegetation at the northbound approach of the Dairy Mart Road/Monument Roadintersection should be maintained periodically. There is a pedestrian crossing sign placed along Monument Road250 feet west of the Dairy Mart Road/Monument Road intersection to warn vehicular traffic of potential pedestriantraffic. As illustrated in the pedestrian and bike counts collected at this intersection (Appendix A), no pedestrianswere observed at this intersection during the AM and PM peak hour; however, three bicyclists were observedcrossing the northbound approach during the AM and the PM peak hour.

All worker and truck traffic will access the site via project access driveway off Monument Road. The crosssection of Monument Road that provides access to the project varies between 26 feet to 40 feet. This section of Monument Road has an undivided travel way and no curb, gutter or sidewalk. An unpaved meandering roadway on the proposed project site would generally provide vehicular travel way to workers and trucks on the site for required sediment management related activities.

As shown in Table 11, the project access intersection would operate at an acceptable LOS.
Table 11. Project Access Peak Hour Intersection LOS

|  |  | AM Peak |  |  | PM Peak |  |
| :--- | :--- | ---: | ---: | :--- | :--- | :---: |
| Intersection | Traffic Control | Delay 1 | LOS $^{2}$ | Delay 1 | LOS $^{2}$ |  |
| Monument Road /Project Access | Stop-control $^{3}$ | 7.4 | A | 8.8 | A |  |

## Notes:

1 Delay is measured in seconds per vehicle
2 Level of Service (LOS)
3 Stop control is not proposed at the Project access point; however, the "driveway" was analyzed assuming people would stop before entering the site. This approach was taken for purposes of traffic software providing a value for LOS.

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## 7 Improvement Measures

Based on the traffic analyses above, the proposed project would not be required to make any off-site improvements to the intersections in the study area.

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Based on the transportation analysis of the proposed project, the following findings on study area intersection levels of service, proposed project trip generation, and opening year conditions are made:

- A daily average of 14 workers, 3 vendor trucks and 6 net new haul trucks would be required for most phases of the project-related activities. The proposed project would generate 46 daily trips, 17 AM peak hour trips ( 17 inbound and 0 outbound), and 17 trips during the PM peak hour ( 0 inbound and 17 outbound). With the application of PCE factors to truck trips, the project would generate 79 total PCE daily trips, and 23 PCE trips during the AM peak hour ( 23 inbound and 0 outbound) and 23 PCE trips during the PM peak hour ( 0 inbound and 23 outbound).
- Based on the small project screening criteria used by State, County and the City, since the project would generate 79 average daily trips, it can be presumed to have a less than significant VMT impact.
- Under Existing and Opening Year conditions, the Hollister Street/Tocayo Avenue intersection operates at LOS F in the AM peak hour and LOS E in the PM peak hour.
- Under Opening Year plus Project conditions, with the addition of project traffic the Hollister Street/Tocayo Avenue intersection would continue to operate at LOS F in the AM peak hour and LOS E in the PM peak hour. However, the proposed project would not add a substantial number of trips to the intersection that would warrant any improvements per the City's guidelines.
- The access to the proposed project would be from Monument Road and the project access driveway would operate at an acceptable LOS under Opening Year plus Project conditions.
- Based on the traffic analyses provided in the memorandum, the proposed project would not be required to make any off-site improvements to the intersections in the study area.

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## 9 References

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SANDAG (San Diego Association of Governments). 2002. Brief Guide of Vehicular Trip Generation Rates for the San Diego Region. April 2002.

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## APPENDIX A Traffic Counts

INTERSECTION TURNING MOVEMENT COUNTS


AimTD LLC
TURNING MOVEMENT COUNTS


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INTERSECTION TURNING MOVEMENT COUNTS

| $\sum_{<}$ | 7:00 AM |
| :---: | :---: |
|  | 7:15 AM |
|  | 7:30 AM |
|  | 7:45 AM |
|  | 8:00 AM |
|  | 8:15 AM |
|  | 8:30 AM |
|  | 8:45 AM |
|  | 9:00 AM |
|  | 9:15 AM |
|  | 9:30 AM |
|  | 9:45 AM |
|  | TOTAL |
| $\sum_{\mathrm{L}}$ | 3:00 PM |
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|  | 4:30 PM |
|  | 4:45 PM |
|  | 5:00 PM |
|  | 5:15 PM |
|  | 5:30 PM |
|  | 5:45 PM |
|  | TOTAL |


| ALL PED AND BIKE |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| N SIDE | S SIDE | E SIDE | W SIDE | TOTAL |  |
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| 0 | 1 | 0 | 0 | 1 |  |
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| PEDESTRIAN CROSSINGS |  |  |  |  |
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| N SIDE | S SIDE | E SIDE | W SIDE | TOTAL |
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| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
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| BICYCLE CROSSINGS |  |  |  |  |
| :---: | :--- | :--- | :--- | :--- |
| NS | SS | ES | WS | TOTAL |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 1 | 0 | 0 | 1 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 1 | 0 | 0 | 0 | 1 |
| 1 | 0 | 0 | 0 | 1 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 2 | 1 | 0 | 0 | 3 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 1 | 0 | 0 | 1 |
| 1 | 0 | 0 | 0 | 1 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 1 | 1 | 0 | 0 | 2 |



## INTERSECTION TURNING MOVEMENT COUNTS

PREPARED BY: AimTD LLC. tel: 7142537888 cs@aimtd.com


## INTERSECTION TURNING MOVEMENT COUNTS



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| U-TURNS |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| NB | SB | EB | WB | TTL |  |
| 0 | 0 | 0 | 0 | 0 |  |
| 0 | 0 | 0 | 0 | 0 |  |
| 0 | 0 | 0 | 0 | 0 |  |
| 0 | 0 | 0 | 0 | 0 |  |
| 0 | 0 | 0 | 0 | 0 |  |
| 0 | 0 | 0 | 0 | 0 |  |
| 0 | 0 | 0 | 0 | 0 |  |
| 0 | 0 | 0 | 0 | 0 |  |
| 0 | 0 | 0 | 0 | 0 |  |
| 0 | 0 | 0 | 0 | 0 |  |
| 0 | 0 | 0 | 0 | 0 |  |
| 0 | 0 | 0 | 0 | 0 |  |
| 0 | 0 | 0 | 0 | 0 |  |


| 0 | 0 | 0 | 0 | 0 |
| :--- | :--- | :--- | :--- | :--- |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |


$\square$

San Ysidro
WEST SIDE
$\square$ SOUTH SIDE

I-5 NB Ramps

San Ysidro
EAST SIDE San Ysidro

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AimTD LLC
TURNING MOVEMENT COUNTS


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PREPARED BY: AimTD LLC. tel: 7142537888 cs@aimtd.com


DATE: Tuesday, January 28, 2020

| $\begin{gathered} \hline \text { AM } \\ \text { TIME } \\ \hline \end{gathered}$ | NORTHBOUND |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | TOTAL | T |
| 0:00 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 1 |
| 0:15 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 12 |
| 0:30 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 |
| 0:45 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 1:00 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 13 |
| 1:15 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 13 |
| 1:30 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 13 |
| 1:45 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 1 |
| 2:00 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 |
| 2:15 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 2:30 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 14, |
| 2:45 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 1 |
| 3:00 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 1 |
| 3:15 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 15 |
| 3:30 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 15 |
| 3:45 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 15 |
| 4:00 | 0 | 11 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 1 |
| 4:15 | 0 | 18 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20 | 1 |
| 4:30 | 0 | 18 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20 | 1 |
| 4:45 | 0 | 18 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 26 | 1 |
| 5:00 | 0 | 20 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 31 | 1 |
| 5:15 | 0 | 25 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 33 | 1 |
| 5:30 | 0 | 34 | 11 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 47 | 1 |
| 5:45 | 1 | 28 | 11 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 41 | 1 |
| 6:00 | 0 | 33 | 16 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 51 | 1 |
| 6:15 | 0 | 29 | 5 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 36 | 1 |
| 6:30 | 1 | 45 | 14 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 61 | 1 |
| 6:45 | 0 | 51 | 15 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 68 | 1 |
| 7:00 | 0 | 66 | 12 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 81 | 1 |
| 7:15 | 0 | 71 | 14 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 89 | 1 |
| 7:30 | 0 | 75 | 10 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 86 | 1 |
| 7:45 | 0 | 66 | 7 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 76 | 1 |
| 8:00 | 0 | 63 | 13 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 78 | 2 |
| 8:15 | 0 | 52 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 64 | 2 |
| 8:30 | 0 | 41 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 51 | 2 |
| 8:45 | 1 | 39 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 48 | 2 |
| 9:00 | 0 | 45 | 9 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 57 | 2 |
| 9:15 | 0 | 26 | 7 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 40 | 2 |
| 9:30 | 0 | 33 | 14 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 48 | 2 |
| 9:45 | 0 | 28 | 7 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 37 | 2 |
| 10:00 | 0 | 33 | 7 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 43 |  |
| 10:15 | 0 | 48 | 10 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 61 | 2 |
| 10:30 | 0 | 39 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 2 |
| 10:45 | 0 | 46 | 7 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 55 | 2 |
| 11:00 | 0 | 44 | 10 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 56 | 2 |
| 11:15 | 0 | 58 | 8 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 69 |  |
| 11:30 | 0 | 48 | 8 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 58 | 2 |
| 11:45 | 1 | 54 | 9 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 69 | 2 |
| TOTAL | 4 | 1,356 | 301 | 6 | 39 | 6 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 1,717 | T |


| AM PEAK HOUR |
| :--- |
| AM PEAK VOLUME |

LOCATION\# San Diego
LOCATION\# San Diego
CLASS1 Dairy Mart between I-5 and Camino De La Plaza

| $\begin{array}{\|c\|} \hline \text { PM } \\ \text { Time } \\ \hline \end{array}$ | NORTHBOUND |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | TOTAL |
| 12:00 | 0 | 67 | 5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 73 |
| 12:15 | 0 | 80 | 9 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 92 |
| 12:30 | 0 | 65 | 7 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 77 |
| 12:45 | 0 | 69 | 10 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 80 |
| 13:00 | 1 | 75 | 14 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 94 |
| 13:15 | 1 | 67 | 10 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 81 |
| 13:30 | 1 | 80 | 14 | 0 | 3 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 100 |
| 13:45 | 0 | 70 | 14 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 88 |
| 14:00 | 1 | 77 | 8 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 87 |
| 14:15 | 0 | 91 | 10 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 105 |
| 14:30 | 0 | 96 | 13 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 111 |
| 14:45 | 0 | 83 | 9 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 94 |
| 15:00 | 0 | 87 | 10 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 104 |
| 15:15 | 0 | 80 | 13 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 94 |
| 15:30 | 0 | 69 | 10 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 80 |
| 15:45 | 0 | 71 | 13 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 87 |
| 16:00 | 1 | 79 | 13 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 95 |
| 16:15 | 0 | 75 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 87 |
| 16:30 | 0 | 70 | 11 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 83 |
| 16:45 | 0 | 78 | 10 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 90 |
| 17:00 | 0 | 81 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 98 |
| 17:15 | 0 | 77 | 19 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 98 |
| 17:30 | 0 | 87 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 105 |
| 17:45 | 0 | 90 | 14 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 105 |
| 18:00 | 0 | 77 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 87 |
| 18:15 | 0 | 53 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 59 |
| 18:30 | 0 | 75 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 85 |
| 18:45 | 0 | 55 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 71 |
| 19:00 | 0 | 50 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 59 |
| 19:15 | 0 | 59 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 70 |
| 19:30 | 0 | 51 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 54 |
| 19:45 | 0 | 45 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 50 |
| 20:00 | 0 | 72 | 12 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 85 |
| 20:15 | 0 | 34 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 37 |
| 20:30 | 0 | 39 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 40 |
| 20:45 | 0 | 27 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 29 |
| 21:00 | 0 | 29 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 34 |
| 21:15 | 0 | 44 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 46 |
| 21:30 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 28 |
| 21:45 | 0 | 37 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 44 |
| 22:00 | 0 | 28 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 31 |
| 22:15 | 0 | 11 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 |
| 22:30 | 0 | 13 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 |
| 22:45 | 0 | 8 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 23:00 | 0 | 9 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 23:15 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 23:30 | 0 | 8 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 23:45 | 0 | 3 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| TOTAL | 5 | 2,725 | 397 | 8 | 41 | 6 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 3,185 |
|  |  |  |  |  |  |  |  |  |  | $\begin{array}{\|l\|} \hline \mathbf{P M} \mathbf{P} \\ \mathbf{P M ~ P} \end{array}$ | $\begin{aligned} & \overline{\text { AK HC }} \\ & \text { AK VO } \end{aligned}$ | $\begin{aligned} & \overline{\text { UR }} \\ & \text { LUME } \end{aligned}$ |  | $\begin{gathered} \hline 2: 15 \mathrm{PM} \\ 414 \end{gathered}$ |


| CLASS 1 | Class 1 - Motorcycles | CLASS 8 | 3 to 4 Axles, Single Trailer |
| :--- | :--- | :--- | :--- |
| CLASS 2 | Passenger Cars | CLASS 9 | 5 Axles, Single Trailer |
| CLASS 3 | 2 Axles, 4-Tire Single Units | CLASS 10 | 6 or More Axles, Single Trailer |
| CLASS 4 | Buses, | CLASS 11 | 5 or Less Axles, Multi-Trailers |
| CLASS 5 | 2 Axles, 6-Tire Single Units | CLASS 12 | 6 Axles, Multi-Trailers |
| CLASS 6 | 3 Axles, Single Unit | CLASS 13 | 7 or More Axles, Multi-Trailers |
| CLASS 7 | 4 or More Axles, Single Unit |  |  |


| TOTAL: AM+PM | 9 | 4,081 | 698 | 14 | 80 | 12 | 0 | 1 | 7 | 0 | 0 | 0 | 0 | 4,902 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% OF TOTAL | $0.2 \%$ | $83.3 \%$ | $14.2 \%$ | $0.3 \%$ | $1.6 \%$ | $0.2 \%$ | $0.0 \%$ | $0.0 \%$ | $0.1 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $100.0 \%$ |
| Class | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ | $\mathbf{1 0}$ | $\mathbf{1 1}$ | $\mathbf{1 2}$ | $\mathbf{1 3}$ |  |




PREPARED BY: AimTD LLC. tel: 7142537888 cs@aimtd.com
DATE: Tuesday, January 28, 2020

```
LOCATION\# San Diego
```

| $\begin{gathered} \hline \text { AM } \\ \text { TIME } \end{gathered}$ | NORTHBOUND |  |  |  |  |  |  |  |  |  |  |  |  |  | PM | NORTHBOUND |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | TOTAL | Time | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 |  |
| 0:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:00 | 0 | 5 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 0:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | , | 0 | 0 | 0 | 0 | 0 | 12:15 | 0 | 9 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 0:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:30 | 0 | 6 | 3 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| 0:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:45 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 1:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 13:00 | 0 | 8 | 8 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 |
| 1:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:15 | 1 | 4 | 5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 1:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:30 | 0 | 7 | 2 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 1:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:45 | 0 | 4 | 4 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 2:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14:00 | 0 | 8 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 2:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14:15 | 0 | 12 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 |
| 2:30 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 14:30 | 0 | 8 | 4 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 |
| 2:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14:45 | 0 | 4 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 3:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15:00 | 0 | 7 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 3:15 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 15:15 | 0 | 5 | 5 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 3:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15:30 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 3:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15:45 | 0 | 5 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 4:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16:00 | 1 | 13 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 |
| 4:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16:15 | 0 | 6 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| 4:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16:30 | 0 | 6 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 4:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16:45 | 0 | 12 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 18 |
| 5:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 17:00 | 1 | 9 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 |
| 5:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17:15 | 0 | 8 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 |
| 5:30 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 17:30 | 0 | 4 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 5:45 | 0 | 1 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 17:45 | 0 | 5 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 6:00 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 18:00 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 6:15 | 0 | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 18:15 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 6:30 | 0 | 4 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 18:30 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 6:45 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 18:45 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 7:00 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 19:00 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 7:15 | 0 | 1 | 3 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 19:15 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 7:30 | 0 | 2 | 5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 19:30 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 7:45 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 19:45 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:00 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 4 | 20:00 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 8:15 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 20:15 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:30 | 0 | 3 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 20:30 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:45 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 20:45 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 9:00 | 0 | 8 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 21:00 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 9:15 | 0 | 3 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 21:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:30 | 0 | 5 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 21:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 | 0 | 2 | 4 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 21:45 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 10:00 | 0 | 1 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 22:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:15 | 0 | 4 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 22:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:30 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 22:30 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 10:45 | 0 | 7 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 22:45 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 11:00 | 1 | 4 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 23:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 11:15 | 0 | 5 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 23:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 | 0 | 3 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 23:30 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 11:45 | 0 | 10 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 23:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL | 1 | 90 | 57 | 0 | 26 | 6 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 181 | TOTAL | 3 | 199 | 94 | 0 | 13 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 314 |
|  |  |  |  |  |  |  |  |  | AM PEAK HOUR $9: 00 \mathrm{AM}$ <br> AM PEAK VOLUME 40 |  |  |  |  |  | PM PEAK HOUR $4: 00$ PM <br> PM PEAK VOLUME 58 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| CLASS 1 | Class 1 - Motorcycles | CLASS 8 | 3 to 4 Axles, Single Trailer |
| :--- | :--- | :--- | :--- |
| CLASS 2 | Passenger Cars | CLASS | 5 Axles, Single Trailer |
| CLASS 3 | 2 Axles, 4-Tire Single Units | CLASS 10 | 6 or More Axles, Single Trailer |
| CLASS 4 | Buses | CLASS 11 | 5 or Less Axles, Multi-Trailers |
| CCASS 5 | 2 Axles, 6-Tire Single Units | CLASS 12 | 6 Axles, Multi-Trailers |
| CLASS 6 | 3 Axles, Single Unit | CLASS 13 | 7 or More Axles, Multi-Trailers |
| CLASS 7 | 4 or More Axles, Single Unit |  |  |


| TOTAL: AM+PM | 4 | 289 | 151 | 0 | 39 | 11 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 495 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% OF TOTAL | $0.8 \%$ | $58.4 \%$ | $30.5 \%$ | $0.0 \%$ | $7.9 \%$ | $2.2 \%$ | $0.0 \%$ | $0.0 \%$ | $0.2 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $100.0 \%$ |
| Class | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ | $\mathbf{1 0}$ | $\mathbf{1 0}$ | $\mathbf{1 1}$ | $\mathbf{1 2}$ | $\mathbf{1 3}$ |


DATE: Tuesday, January 28, 2020 LOCATION\# San Diego

| $\begin{array}{\|c\|} \hline \text { AM } \\ \text { TIME } \\ \hline \end{array}$ | EASTBOUND |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{gathered} \hline \text { PM } \\ \text { Time } \\ \hline \end{gathered}$ | EASTBOUND |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | TOTAL |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | TOTAL |
| 0:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:00 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 0:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:15 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 0:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:30 | 0 | 7 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 0:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:45 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 1:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:00 | 0 | 7 | 5 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 |
| 1:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:15 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 1:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:30 | 1 | 3 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 1:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:45 | 0 | 3 | 3 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 2:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14:00 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 2:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14:15 | 0 | 12 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 |
| 2:30 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 14:30 | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 2:45 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 14:45 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 3:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15:00 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 3:15 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 15:15 | 0 | 4 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 3:30 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 15:30 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 3:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15:45 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 4:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 16:00 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 4:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16:15 | 0 | 4 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 4:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16:30 | 0 | 2 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 4:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16:45 | 0 | 12 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 |
| 5:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17:00 | 0 | 9 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| 5:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17:15 | 0 | 9 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 |
| 5:30 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 17:30 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 5:45 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 17:45 | 1 | 2 | , | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 6:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 18:00 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 6:15 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 18:15 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 6:30 | 0 | 2 | 2 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 18:30 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 6:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 18:45 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 7:00 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 19:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 | 0 | 2 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 19:15 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 7:30 | 0 | 3 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 19:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 19:45 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 8:00 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 20:00 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 8:15 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 20:15 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:30 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 20:30 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:45 | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 20:45 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 9:00 | 0 | 4 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 21:00 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 9:15 | 0 | 2 | 5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 21:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:30 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 21:30 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 9:45 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 21:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:00 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 22:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:15 | 0 | 6 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 22:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:30 | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 22:30 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 10:45 | 0 | 5 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 22:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 23:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 11:15 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 23:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 23:30 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 11:45 | 0 | 7 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 23:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL | 0 | 75 | 36 | 0 | 6 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 123 | TOTAL | 2 | 134 | 53 | 0 | 4 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 197 |
|  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { AM PE } \\ & \text { AM PE } \end{aligned}$ | AK HO | $\begin{aligned} & \overline{\text { UR }} \\ & \text { UME } \end{aligned}$ |  | $\begin{gathered} \hline 10: 15 \mathrm{AM} \\ 28 \\ \hline \end{gathered}$ |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { PM PE } \\ & \text { PM PE } \end{aligned}$ | AK HO AK VO | $\begin{aligned} & \text { UR } \\ & \text { LUME } \end{aligned}$ |  | $\begin{gathered} \hline 4: 30 \mathrm{PM} \\ 46 \end{gathered}$ |
| CLASS 1 |  | Class 1 - | torcy |  |  | CLAS |  | 3 to 4 | xles, | Single | railer |  |  | TOTAL: A | M+PM | 2 | 209 | 89 | 0 | 10 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 320 |
| CLASS 2 |  | Passenge |  |  |  | CLAS |  | 5 Axle | Sing | le Trail |  |  |  | \% OF TO | TAL | 0.6\% | 65.3\% | 27.8\% | 0.0\% | 3.1\% | 3.1\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 100.0\% |
| CLASS 3 |  | 2 Axles, | e Sing | Units |  | CLAS |  | 6 or M | re Ax | xles, Sin | Tra |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| CLASS 4 CLASS 5 |  | Buses 2 Axles, |  | Units |  | $\begin{aligned} & \text { CLAS } \\ & \text { CLAS } \end{aligned}$ |  | $\begin{aligned} & 5 \text { or Le } \\ & 6 \text { Axle } \end{aligned}$ | $\begin{aligned} & \text { ss Axl } \\ & \text { Mult } \end{aligned}$ | es, Mult i-Traile | Traile |  |  | Class |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 |  |
| CLASS 6 |  | 3 Axles, | le Uni |  |  | CLAS |  | 7 or M | a Ax | les, Mu | -Trail |  |  | TOTAL: A |  | 5 | 460 | 188 | 0 | 29 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 702 |
| CLASS 7 |  | 4 or More | les, Si | gle Unit |  |  |  |  |  |  |  |  |  | \% OF TO |  | 1.6\% | 143.8\% | 58.8\% | 0.0\% | 9.1\% | 6.3\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 100.0\% |


DATE: Tuesday, January 28, 2020 LOCATION\# San Diego

| $\begin{array}{\|c\|} \hline \text { AM } \\ \hline \text { TIME } \\ \hline \end{array}$ | EASTBOUND |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{\|c\|} \hline \text { PM } \\ \text { Time } \\ \hline \end{array}$ | EASTBOUND |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 1 | 12 | 13 | TOTAL |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | TOTAL |
| 0:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:00 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 0:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:15 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 0:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:30 | 0 | 3 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 0:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:45 | 1 | 5 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 1:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:00 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 1:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:15 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 1:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:30 | 1 | 1 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 1:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:45 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 2:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14:00 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 2:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14:15 | 0 | 9 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 2:30 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 14:30 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 2:45 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 14:45 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 3:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15:00 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 3:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15:15 | 0 | 3 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 3:30 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 15:30 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 3:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15:45 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 4:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16:00 | 0 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 4:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16:15 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 4:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16:30 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 4:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16:45 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 5:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17:00 | 0 | 8 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 5:15 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 17:15 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 5:30 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 17:30 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 5:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17:45 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 6:00 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 18:00 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 6:15 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 18:15 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 6:30 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 18:30 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 6:45 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 18:45 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 7:00 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 19:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 19:15 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 7:30 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 19:30 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 7:45 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 19:45 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 8:00 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 20:00 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 8:15 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 20:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 20:30 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:45 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 20:45 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 9:00 | 0 | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 21:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 21:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:30 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 21:30 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 9:45 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 21:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:00 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 22:00 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 10:15 | 0 | 5 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 22:15 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 10:30 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 22:30 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 10:45 | 0 | 3 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 22:45 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 11:00 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 23:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:15 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 23:15 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 11:30 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 23:30 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 11:45 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 23:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL | 0 | 46 | 24 | 0 | 3 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 77 | TOTAL | 3 | 106 | 55 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 167 |
|  |  |  |  |  |  |  |  |  |  | $\overline{A M P E P E E}$ | $\begin{aligned} & \mathbf{K H O} \\ & \mathrm{K} \mathbf{0} \end{aligned}$ |  |  | $\begin{gathered} 10: 00 \mathrm{AM} \\ 21 \end{gathered}$ |  |  |  |  |  |  |  |  |  |  | $\begin{array}{\|l\|} \hline \mathbf{P M ~ P I} \\ \text { PM PI } \end{array}$ | $\begin{aligned} & \overline{A K ~ H C} \\ & A K V O \end{aligned}$ | $\begin{aligned} & \text { UR } \\ & \text { LUME } \end{aligned}$ |  | $\begin{array}{r} \hline 2: 00 \mathrm{PM} \\ \hline \end{array}$ |
| CLASS 1 |  | Class 1 - | torcy |  |  | CLAS |  | 3 to 4 | xles, | ingle |  |  |  | TOTAL: A | M+PM | 3 | 152 | 79 | 0 | 4 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 244 |
| CLASS 2 |  | Passenge |  |  |  | CLAS |  | 5 Axle | Sing | Trail |  |  |  | \% OF TO | TAL | 1.2\% | 62.3\% | 32.4\% | 0.0\% | 1.6\% | 2.5\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 100.0\% |
| CLASS 3 |  | 2 Axles, 4 | e Sin | Units |  | CLAS |  | 6 or M | Ax | s, Sin | Tra |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & \text { CLASS } 4 \\ & \text { CLASS } 5 \end{aligned}$ |  | Buses 2 Axles, | e Sin | Units |  | $\begin{aligned} & \text { CLAS } \\ & \text { CLAS } \end{aligned}$ |  | $\begin{aligned} & 5 \text { or Le } \\ & 6 \text { Axle } \end{aligned}$ |  | S, Mult | raile |  |  | Class |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 |  |
| CLASS 6 |  | 3 Axles, | le Un |  |  | CLAS |  | 7 or M | Ax | s, Mu | rail |  |  | TOTAL: A |  | 6 | 338 | 160 | 0 | 13 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 529 |
| CLASS 7 |  | 4 or More | les, | e Unit |  |  |  |  |  |  |  |  |  | \% OF TO | TAL | 2.5\% | 138.5\% | 65.6\% | 0.0\% | 5.3\% | 4.9\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 100.0\% |



DATE: Tuesday, January 28, 2020

| AM | NORTHBOUND |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{\|c\|} \hline \text { PM } \\ \text { Time } \\ \hline \end{array}$ | NORTHBOUND |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TIME | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | TOTAL |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | TOTAL |
| 0:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 12:00 | 0 | 22 | 6 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 29 |
| 0:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:15 | 0 | 19 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 22 |
| 0:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:30 | 0 | 18 | 4 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 23 |
| 0:45 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 2 | 12:45 | 0 | 13 | 2 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 |
| 1:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:00 | 0 | 14 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 |
| 1:15 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 13:15 | 0 | 20 | 7 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 30 |
| 1:30 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 13:30 | 0 | 20 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 |
| 1:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:45 | 0 | 20 | 4 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 26 |
| 2:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 14:00 | 0 | 20 | 14 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 35 |
| 2:15 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 14:15 | 0 | 33 | 13 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 48 |
| 2:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14:30 | 1 | 24 | 10 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 36 |
| 2:45 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 14:45 | 1 | 28 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 38 |
| 3:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 15:00 | 0 | 21 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 36 |
| 3:15 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 15:15 | 0 | 31 | 7 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 39 |
| 3:30 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 15:30 | 0 | 26 | 4 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 31 |
| 3:45 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 15:45 | 1 | 16 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 35 |
| 4:00 | 0 | 3 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 16:00 | 0 | 20 | 16 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 37 |
| 4:15 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 16:15 | 2 | 15 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 |
| 4:30 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 16:30 | 0 | 24 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 37 |
| 4:45 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 16:45 | 0 | 20 | 17 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 39 |
| 5:00 | 1 | 7 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 17:00 | 0 | 17 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 23 |
| 5:15 | 0 | 10 | 8 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 17:15 | 1 | 26 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 39 |
| 5:30 | 0 | 9 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 17:30 | 0 | 17 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 29 |
| 5:45 | 0 | 8 | 5 | 0 | 1 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 18 | 17:45 | 0 | 26 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 38 |
| 6:00 | 0 | 10 | 5 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 18:00 | 0 | 26 | 12 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 40 |
| 6:15 | 0 | 9 | 4 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 17 | 18:15 | 0 | 22 | 11 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 35 |
| 6:30 | 1 | 24 | 9 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 35 | 18:30 | 2 | 11 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 |
| 6:45 | 2 | 36 | 8 | 1 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 52 | 18:45 | 0 | 19 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 25 |
| 7:00 | 1 | 46 | 5 | 1 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 60 | 19:00 | 0 | 14 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 |
| 7:15 | 0 | 24 | 7 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 36 | 19:15 | 0 | 11 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 |
| 7:30 | 1 | 17 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 27 | 19:30 | 0 | 8 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| 7:45 | 2 | 34 | 7 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 19:45 | 0 | 8 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| 8:00 | 0 | 16 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 25 | 20:00 | 0 | 11 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 |
| 8:15 | 0 | 17 | 5 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 20:15 | 0 | 10 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| 8:30 | 0 | 12 | 5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 18 | 20:30 | 0 | 16 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 |
| 8:45 | 0 | 14 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 20:45 | 0 | 9 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 9:00 | 0 | 23 | 5 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 29 | 21:00 | 0 | 6 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 9:15 | 0 | 11 | 4 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 21:15 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 9:30 | 0 | 12 | 4 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 21:30 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 9:45 | 0 | 12 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 21:45 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 10:00 | 0 | 16 | 6 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 25 | 22:00 | 2 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 10:15 | 0 | 11 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 22:15 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 10:30 | 0 | 12 | 2 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 22:30 | 4 | 9 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 |
| 10:45 | 0 | 21 | 5 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 27 | 22:45 | 0 | 10 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 11:00 | 0 | 12 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 23:00 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 11:15 | 1 | 20 | 7 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 30 | 23:15 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 11:30 | 0 | 14 | 4 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20 | 23:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 | 1 | 17 | 3 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 23:45 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| TOTAL | 10 | 504 | 155 | 4 | 28 | 16 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 723 | TOTAL | 14 | 727 | 291 | 5 | 15 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1,060 |
|  |  |  |  |  |  |  |  |  |  | AM P AM P | AK | $\begin{aligned} & \text { UR } \\ & \text { LUME } \end{aligned}$ |  | $\begin{array}{\|} \hline 6: 30 \mathrm{AM} \\ 183 \\ \hline \end{array}$ |  |  |  |  |  |  |  |  |  |  | PM P PM PE | $\overline{\mathrm{AKHC}}$ | $\begin{aligned} & \text { JR } \\ & \text { UME } \end{aligned}$ |  | $\begin{gathered} \hline 2: 15 \mathrm{PM} \\ 158 \end{gathered}$ |


| TOTAL: AM+PM | 24 | 1,231 | 446 | 9 | 43 | 24 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 1,783 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% OF TOTAL | $1.3 \%$ | $69.0 \%$ | $25.0 \%$ | $0.5 \%$ | $2.4 \%$ | $1.3 \%$ | $0.0 \%$ | $0.0 \%$ | $0.3 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $100.0 \%$ |

Class

| TOTAL: ALL | 46 | 2,388 | 866 | 19 | 75 | 47 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 3,453 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% OF TOTAL | $2.6 \%$ | $133.9 \%$ | $48.6 \%$ | $1.1 \%$ | $4.2 \%$ | $2.6 \%$ | $0.0 \%$ | $0.0 \%$ | $0.7 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $100.0 \%$ |


DATE: Tuesday, January 28, $2020 \quad$ LOCATION\# San Diego

| $\begin{array}{\|c\|} \hline \text { AM } \\ \text { TIME } \\ \hline \end{array}$ | NORTHBOUND |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{gathered} \hline \text { PM } \\ \text { Time } \\ \hline \end{gathered}$ | NORTHBOUND |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | TOTAL |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | TOTAL |
| 0:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:00 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 0:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:15 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 0:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:30 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 0:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12:45 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 1:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:00 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 1:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:15 | 0 | 0 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 1:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:30 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 1:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13:45 | 0 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 2:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14:00 | 0 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 2:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14:15 | 0 | 9 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 2:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14:30 | 1 | 10 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| 2:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14:45 | 0 | 10 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| 3:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15:00 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 3:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15:15 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 3:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15:30 | 0 | 6 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 3:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15:45 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 4:00 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 16:00 | 0 | 2 | 5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 4:15 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 16:15 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 4:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16:30 | 0 | 3 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 4:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16:45 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 5:00 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 17:00 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 5:15 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 17:15 | 1 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 5:30 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 17:30 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 5:45 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 17:45 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 6:00 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 18:00 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 6:15 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 18:15 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 6:30 | 1 | 11 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 18:30 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 6:45 | 0 | 6 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 18:45 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 7:00 | 0 | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 19:00 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 7:15 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 19:15 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 7:30 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 19:30 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 7:45 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 19:45 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:00 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 20:00 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 8:15 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 20:15 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 8:30 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 20:30 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 8:45 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 20:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 | 0 | 3 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 21:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 9:15 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 21:15 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 9:30 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 21:30 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 9:45 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 21:45 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 10:00 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 22:00 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 10:15 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 22:15 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 10:30 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 22:30 | 4 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| 10:45 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 22:45 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 11:00 | 1 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 23:00 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 11:15 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 23:15 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 11:30 | 0 | 3 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 23:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 | 0 | 4 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 23:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL | 2 | 69 | 28 | 0 | 6 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 110 | TOTAL | 9 | 151 | 65 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 227 |
|  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \hline \mathbf{A M ~ P E} \\ & \text { AM PE } \end{aligned}$ | $\begin{aligned} & \overline{B A K ~ H} \\ & =\Delta K ~ V \end{aligned}$ | $\begin{aligned} & \text { UR } \\ & \text { LUME } \end{aligned}$ |  | $\begin{array}{\|c} \hline 6: 30 \mathrm{AM} \\ 28 \\ \hline \end{array}$ |  |  |  |  |  |  |  |  |  |  | PM P PM P |  | UME |  | $\begin{array}{\|c\|} \hline 2: 00 \mathrm{PM} \\ 44 \end{array}$ |


| CLASS 1 | Class 1 - Motorcycles | CLASS 8 | 3 to 4 4xles, Single Trailer |
| :--- | :--- | :--- | :--- |
| CLASS 2 | Passenger Cars | CLASS 9 | 5 Axles, Single Trailer |
| CLASS 3 | 2 Axles, 4-Tire Single Units | CLASS 10 | 6 or More Axles, Single Trailer |
| CLASS 4 | Buses | CLASS 11 | 5 or Less Axxes, Multi-Trailers |
| CLASS 5 | 2 Axles, 6-Tire Single Units | CLASS 12 | 6 Axles, Multi-Trailers |
| CLASS 6 | 3 Axles, Single Unit | CLASS 13 | 7or More Axles, Multi-Trailers |
| CLASS 7 | 4 or More Axles, Single Unit |  |  |


| TOTAL: AM+PM | 11 | 220 | 93 | 0 | 7 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 337 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% OF TOTAL | $3.3 \%$ | $65.3 \%$ | $27.6 \%$ | $0.0 \%$ | $2.1 \%$ | $1.8 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $100.0 \%$ |
| Class | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ | $\mathbf{1 0}$ | $\mathbf{1 1}$ | $\mathbf{1 2}$ | $\mathbf{1 3}$ |  |



|  | INTERVAL | PHASE TIMINC |  |  |  |  |  |  |  | 9 | $\begin{gathered} \text { PRE-EMPTION } \\ \text { E } \end{gathered}$ |  | F |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  | ELAGS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |
| 0 | WALK | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | CLK RST | EYSET | 0 | RPRUP |  | 2 |  | 4 | 5 | 6 |  |  | 0 |
| 1 | DONT WALK | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |  | RR1 CLR | 5 | RED LOCK |  |  |  |  |  |  |  |  | 1 |
| 2 | MIN GREEN | 1 | 5 | 1 | 5 | 5 | 5 | 1 | 1 |  | EVA DLY | 0 | YEL LOCK |  |  |  |  |  |  |  |  | 2 |
| 3 | TYPE 3 DET | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | EVA CLR | 5 | V RECALL |  | 2 |  |  |  | 6 |  |  | 3 |
| 4 | ADD/VEH | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | EVB DLY | 0 | P RECALL |  |  |  |  |  |  |  |  | 4 |
| 5 | PASSAGE | 0.9 | 6.2 | 0.9 | 2.0 | 2.0 | 6.2 | 9.0 | 0.9 |  | EVB CLR | 5 | PETPRHASES |  |  |  |  |  |  |  |  | 5 |
| 6 | MAX GAP | 0.9 | 8.2 | 0.9 | 2.0 | 2.0 | 8.2 | 9.0 | 0.9 |  | EVC DLY | 0 | RT OLA |  |  |  |  |  |  |  |  | 6 |
| 7 | MIN GAP | 0.9 | 3.0 | 0.9 | 2.0 | 2.0 | 3.0 | 9.0 | 0.9 |  | EVC CLR | 5 | RT OLB |  |  |  |  |  |  |  |  | 7 |
| 8 | MAX EXT | 9 | 35 | 9 | 25 | 25 | 35 | 9 | 9 |  | EVD DLY | 0 | DBL ENTRY |  |  |  |  |  |  |  |  | 8 |
| 9 | MAX 2 |  |  |  |  |  |  |  |  | YR | EVD CLR | 5 | MAX 2 PH |  |  |  |  |  |  |  |  | 9 |
| A | MAX 3 |  |  |  |  |  |  |  |  | MO | MAX EV | 255 | LAG PHI SES |  |  |  | 4 | © | Tr |  |  | A |
| B |  |  |  |  |  |  |  |  |  | DAY | RR2 CLR | 5 | RED RES |  |  |  |  |  |  |  |  | B |
| C | REDUCE BY | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | DOW |  |  | R ${ }^{\text {ST TV WALK }}$ |  |  |  |  |  |  |  |  | C |
| D | EVERY | 1.0 | 0.5 | 1.0 | 1.0 | 1.0 | 0.5 | 1.0 | 1.0 | HR |  |  | A A 3 PIIASES |  |  |  |  |  |  |  |  | D |
| E | YELLOW | 3.0 | 4.1 | 3.0 | 4.1 | 3.7 | 4.1 | 3.0 | 3.0 | MIN |  |  | YEL START UP |  | 2 |  |  |  | 6 |  |  | E |
| F | RED | 0.0 | 1.0 | 0.0 | 1.0 | 1.0 | 1.0 | 0.0 | 0.0 | SEC |  |  | H RST PHASE |  |  |  | 4 |  |  |  |  | F |
|  | PED XING FT |  |  |  |  |  |  |  |  |  |  |  |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |
|  | NOTES : | $\mathrm{MPH}=35$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| FOC LONG FAILURE |  |
| :---: | :---: |
| FOD SHORT FAILURE |  |
| FOE | 0 |
| FOF | 5 |
| FCO | 3 |
| FC1 | 3 |
| FC2 | 10 |
| FCA | 3.0 |
| FCB | 0.0 |
| FCC | 2.0 |
| FCD | 0.0 |


| FDO | TB SELECT | $\mathbf{1}$ |
| :--- | :--- | :--- |
| FD3 PED SELECT | 0 |  |
| FD4 7 WIRE | 0 |  |
| FD5 PERMISSIVE | 0 |  |
| FD8 OS SEEKING | 1 |  |


| CO5 | FLASH TYPE | 1 |
| :--- | :--- | :--- |
| CC2 DOWNLOAD | 1 |  |

世

C PAGE

|  |  | CONTROL PLANS |  |  |  |  |  |  |  |  | Y-COORD |  |  | LAG PHASE | FLAGS |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |  | C | D | E | F | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |
| 0 | CYCLE LENGTH |  |  |  |  |  |  |  |  |  |  |  |  |  | LAG FZ FREE |  | 2 |  | 4 |  | 6 |  | 8 | 0 |
| 1 | EZ1 GRN FCTR |  |  |  |  |  |  |  |  |  |  |  |  | GAPOUT CP1 | LAG FZ CP 1 |  |  |  |  |  |  |  |  | 1 |
| 2 |  |  |  |  |  |  |  |  |  |  |  |  |  | GAPOUT CP2 | LAG EZ CP 2 |  |  |  |  |  |  |  |  | 2 |
| 3 | FZ3 GRN FCTR |  |  |  |  |  |  |  |  |  |  |  |  | GAPOUT CP3 | LAG EZ CP 3 |  |  |  |  |  |  |  |  | 3 |
| 4 | FZ4 GRN FCTR |  |  |  |  |  |  |  |  |  | PERM TIME |  |  | GAPOUT CP4 | LAG FZ CP 4 |  |  |  |  |  |  |  |  | 4 |
| 5 | FZ5 GRN FCTR |  |  |  |  |  |  |  |  |  | LAG OFFSET |  |  | GAPOUT | LAG FZ CP 5 |  |  |  |  |  |  |  |  | 5 |
| 6 |  |  |  |  |  |  |  |  |  |  | FORCE OFF |  |  | GAPOUT ${ }^{\text {a }} 6$ | LAG FZ CP 6 |  |  |  |  |  |  |  |  | 6 |
| 7 | FZ7 GRN FCTR |  |  |  |  |  |  |  |  |  | LONG GRN |  |  | GAP UT PP7 | LAG EZ CP 7 |  |  |  |  |  |  |  |  | 7 |
| 8 | FZ8 GRN FCTR |  |  |  |  |  |  |  |  |  | NO GREEN |  |  | GA, QU1 CP8 | LAG EZ CP 8 |  |  |  |  |  |  |  |  | 8 |
| 9 | MULTI CYCLE |  |  |  |  |  |  |  |  |  |  |  |  | DOUT CP9 | LAG FZ CP 9 |  |  |  |  |  |  |  |  | 9 |
| A | OFFSET A |  |  |  |  |  |  |  |  |  | OFESET |  |  |  | LAG C COORD |  |  |  |  |  |  |  |  | A |
| B | OFFSET B |  |  |  |  |  |  |  |  |  |  |  |  |  | LAG D COORD |  |  |  |  |  |  |  |  | B |
| C | OFESET C |  |  |  |  |  |  |  |  |  |  |  |  |  | COORD FAZES |  | 2 |  |  |  | 6 |  |  | C |
| D | EZ 3 EXT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | D |
| E | EZ 7 EXT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | E |
| F | OFFSET INTRPT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | F |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |


$C C B / C D B$ OFFSET TIMER
$C C C / C D C$ LAG GREEN TIMER
$C C D / C D D$ FORCE OFF TIMER
CCE/CDE LONG GREEN TIMER
$C C F / C D F$ NO GREEN TIMER

|  | D | FLAGS |  |  |  |  |  |  |  | E | FLAGS |  |  |  |  |  |  |  | F | FLAGS |  |  |  |  |  |  |  |  | E | FLAGS |  |  |  |  |  |  |  | F | FLAGS |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | MAX | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | MIN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | PED | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  | FUNCTION | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | FUNCTION | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |
| 0 | RCL |  |  |  |  |  |  |  |  | RCL |  |  |  |  |  |  |  |  | RCL |  |  |  |  |  |  |  |  | 0 |  |  |  |  |  |  |  |  |  | CODE 4 |  |  |  |  |  |  |  |  | 0 |
| 1 | CP 1 |  |  |  |  |  |  |  |  | CP 1 |  |  |  |  |  |  |  |  | CP 1 |  |  |  |  |  |  |  |  | 1 |  |  |  |  |  |  |  |  |  | CODE 5 |  |  |  |  |  |  |  |  | 1 |
| 2 | CP 2 |  |  |  |  |  |  |  |  | CP 2 |  |  |  |  |  |  |  |  | CP 2 |  |  |  |  |  |  |  |  | 2 |  |  |  |  |  |  |  |  |  | C-RECALL |  |  |  |  |  |  |  |  | 2 |
| 3 | CP 3 |  |  |  |  |  |  |  |  | CP 3 |  |  |  |  |  |  |  |  | CP 3 |  |  |  |  |  |  |  |  | 3 |  |  |  |  |  |  |  |  |  | D-RECALL |  |  |  |  |  |  |  |  | 3 |
| 4 | CP 4 |  |  |  |  |  |  |  |  | CP 4 |  |  |  |  |  |  |  |  | CP 4 |  |  |  |  |  |  |  |  | 4 |  |  |  |  |  |  |  |  |  | dxequsum |  |  |  |  |  |  |  |  | 4 |
| 5 | CP 5 |  |  |  |  |  |  |  |  | CP 5 |  |  |  |  |  |  |  |  | CP 5 |  |  |  |  |  |  |  |  | 5 |  |  |  |  |  |  |  |  |  | 2 pep |  | 2 |  |  |  |  |  |  | 5 |
| 6 | CP 6 |  |  |  |  |  |  |  |  | CP 6 |  |  |  |  |  |  |  |  | CP 6 |  |  |  |  |  |  |  |  | 6 |  |  |  |  |  |  |  |  |  | G pee |  |  |  |  |  | 6 |  |  | 6 |
| 7 | CP 7 |  |  |  |  |  |  |  |  | CP 7 |  |  |  |  |  |  |  |  | CP 7 |  |  |  |  |  |  |  |  | 7 |  |  |  |  |  |  |  |  |  | 4 HES |  |  |  | 4 |  |  |  |  | 7 |
| 8 | CP 8 |  |  |  |  |  |  |  |  | CP 8 |  |  |  |  |  |  |  |  | CP 8 |  |  |  |  |  |  |  |  | 8 |  |  |  |  |  |  |  |  |  | ¢ exa |  |  |  |  |  |  |  | $8:$ | 8 |
| 9 | CP 9 |  |  |  |  |  |  |  |  | CP 9 |  |  |  |  |  |  |  |  | CP 9 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 9 |
| A |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | RCL 1 |  |  |  |  |  |  |  |  |  | OLA $\Lambda$ - |  |  |  |  |  |  |  |  | Qua en |  |  |  |  |  |  |  |  | A |
| B |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | RCL 2 |  |  |  |  |  |  |  |  |  | QUQ |  |  |  |  |  |  |  |  | OLS ON |  |  |  |  |  |  |  |  | B |
| C |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | C | OLe Nop |  |  |  |  |  |  |  |  | OLOTO |  |  |  |  |  |  |  |  | C |
| D |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | D | ○एण Not |  |  |  |  |  |  |  |  | QRTSovt |  |  |  |  |  |  |  |  | D |
| E |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | E |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | E |
| F |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | F |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | F |
|  |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  | 1 | 2 | 3 | 4 |  |  |  |  |  |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |



| TIME OF DAY ACTIVITY TABLE |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7+EVENT+HR+MIN+ACT+"E"+ON/OFF+DOW LTS |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | ON / | S | M | T | W | T | F | S |
|  | HR | MIN | АСТ | OFF | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 0 |  |  |  |  |  |  |  |  |  |  |  |
| 1 |  |  |  |  |  |  |  |  |  |  |  |
| 2 |  |  |  |  |  |  |  |  |  |  |  |
| 3 |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |  |  |  |  |  |
| 8 |  |  |  |  |  |  |  |  |  |  |  |
| 9 |  |  |  |  |  |  |  |  |  |  |  |
| A |  |  |  |  |  |  |  |  |  |  |  |
| B |  |  |  |  |  |  |  |  |  |  |  |
| C |  |  |  |  |  |  |  |  |  |  |  |
| D |  |  |  |  |  |  |  |  |  |  |  |
| E |  |  |  |  |  |  |  |  |  |  |  |
| F |  |  |  |  |  |  |  |  |  |  |  |

1 TYPE OF MAX TERMINATION
2 MAX 2
3 MAX 3
4 COND SERV (1ST SELECT)
5 COND SERV (2ND SELECT)
6 ENERGIZE AUX OUTPUT-RED

7 ENERGIZE AUX OUTPUT-GREEN

| CON'IROL PLAN TIME OF DAY |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9+EVENT+HR+MIN+CP+OS+E+DOW |  |  |  |  |  |  |  |  |  |  |  |
|  | HR | MIN | CP | OS | S | M | T 3 | W | T T | F | S |
|  |  |  |  |  |  |  |  |  |  |  |  |
| 0 |  |  |  |  |  |  |  |  |  |  |  |
| 1 |  |  |  |  |  |  |  |  |  |  |  |
| 2 |  |  |  |  |  |  |  |  |  |  |  |
| 3 |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |  |  | - | - |  |
| 8 |  |  |  |  |  |  |  |  |  | $\bigcirc$ |  |
| 9 |  |  |  |  |  |  |  |  |  |  |  |
| A |  |  |  |  |  |  |  |  |  |  |  |
| B |  |  |  |  |  | - | $\checkmark$ |  |  |  |  |
| C |  |  |  |  |  | $\bigcirc$ |  |  |  |  |  |
| D |  |  |  |  |  | $\checkmark$ |  |  |  |  |  |
| E |  |  |  |  |  |  |  |  |  |  |  |
| F |  |  |  |  |  |  |  |  |  |  |  |


| CONTROL PLAN TIME OF DAY |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| +EVENT+HR+MIN+CP+OS+E+DOW |  |  |  |  |  |  |  |  |  |  |  |
|  | HR | MIN | CP | OS | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 0 |  |  |  |  |  |  |  |  |  |  |  |
| 1 |  |  |  |  |  |  |  |  |  |  |  |
| 2 |  |  |  |  |  |  |  |  |  |  |  |
| 3 |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |  |  |  |  |  |
| 8 |  |  |  |  |  |  |  |  |  |  |  |
| 9 |  |  |  |  |  |  |  |  |  |  |  |
| A |  |  |  |  |  |  |  |  |  |  |  |
| B |  |  |  |  |  |  |  |  |  |  |  |
| C |  |  |  |  |  |  |  |  |  |  |  |
| D |  |  |  |  |  |  |  |  |  |  |  |
| E |  |  |  |  |  |  |  |  |  |  |  |
| F |  |  |  |  |  |  |  |  |  |  |  |




|  | INTERVAL | 1 | 2 | PIIASE TIMING |  |  |  |  |  | 9 | PRE-EMPTIONE |  | F |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  | FLAGS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |
| 0 | WALK | 1 | 7 | 1 | 7 | 1 | 7 | 1 | 1 | CLK RST | YYSES | 0 | Qeruere | 1 | 2 |  | 4 |  | 6 |  |  | 0 |
| 1 | DONT WALK | 1 | 9 | 1 | 24 | 1 | 14 | 1 | 1 |  | RR1 CLR | 5 | RED LOCK |  |  |  |  |  |  |  |  | 1 |
| 2 | MIN GREEN | 5 | 5 | 1 | 5 | 1 | 5 | 1 | 1 |  | EVA DLY | 0 | YEL LOCK |  |  |  |  |  |  |  |  | 2 |
| 3 | TYPE 3 DET | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | EVA CLR | 5 | V RECALL |  | 2 |  |  |  | 6 |  |  | 3 |
| 4 | ADD/VEH | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | EVB DLY | 0 | P RECALL |  |  |  |  |  |  |  |  | 4 |
| 5 | PASSAGE | 2.0 | 3.9 | 0.9 | 2.0 | 0.9 | 3.9 | 0.9 | 0.9 |  | E'VB CLK | 5 | EQU L |  |  |  | 4 |  | 6 |  |  | 5 |
| 6 | MAX GAP | 2.0 | 5.9 | 0.9 | 2.0 | 0.9 | 5.9 | 0.9 | 0.9 |  | EVC DLY | 0 | RT OLA |  |  |  |  |  |  |  |  | 6 |
| 7 | MIN GAP | 2.0 | 3.0 | 0.9 | 2.0 | 0.9 | 3.0 | 0.9 | 0.9 |  | EVC CLR | 5 | RT OLB |  |  |  |  |  |  |  |  | 7 |
| 8 | MAX EXT | 25 | 30 | 9 | 25 | 9 | 30 | 9 | 9 |  | EVD DLY | 0 | DBL ENTRY |  |  |  |  |  |  |  |  | 8 |
| 9 | MAX 2 |  | 40 |  | 35 |  | 40 |  |  |  | EVD CLR | 5 | MAX 2 PH S |  | 2 |  | 4 |  | 6 |  |  | 9 |
| A | MAX 3 |  |  |  |  |  |  |  |  | MO | MAX EV | 255 | LAG PHI SES |  |  |  | A | 0 | 1 |  |  | A |
| B |  |  |  |  |  |  |  |  |  | DAY | RR2 CLR | 5 | RED RE, |  |  |  |  |  |  |  |  | B |
| C | REDUCE BY | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | DOW |  |  | RपST TV WALK |  |  |  |  |  |  |  |  | C |
| D | EVERY | 1.0 | 0.9 | 1.0 | 1.0 | 1.0 | 0.9 | 1.0 | 1.0 | HR |  |  | 78 3 PHASES |  |  |  |  |  |  |  |  | D |
| E | YELLOW | 3.7 | 4.1 | 3.0 | 4.1 | 3.0 | 4.1 | 3.0 | 3.0 | MIN |  |  | YFE START UP |  | 2 |  |  |  | 6 |  |  | E |
| F | RED | 1.0 | 1.0 | 0.0 | 1.0 | 0.0 | 1.0 | 0.0 | 0.0 | SEC |  |  | E RST PHASE |  |  |  | 4 |  |  |  |  | F |
| $3.5{ }^{\prime}$ | PED XING FT |  | $44^{\prime}$ |  | $98^{\prime}$ |  | $63^{\prime}$ |  |  |  |  |  |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |



| FCO | 3 |
| :---: | :---: |
| FC1 | 3 |
| F'C2 | 10 |
| FCA | 0.0 |
| FCB | 0.0 |
| FCC | 0.0 |
| FCD | 0.0 |


| FDO | TB SELECT | 1 |
| :--- | :--- | :--- |
| FD3 PED SELECT | 0 |  |
| FD4 7 WIRE | 0 |  |
| FD5 PERMISSIVE | 0 |  |
| FD8 OS SEEKING | 1 |  |


| CO5 FLASH TYPE | 1 |
| :--- | :--- |
| CC2 DOWNLOAD | 1 |



CO1 MANUAL CP
CO2 MASTER CP
CO3 CURRENT CP
CO4 LAST CP
CO7 TRNSMT CP
COD MANUAL OFFSET
CAO LOCAL CYCLE TIMER
CBO MASTER CYCLE TIMER
CAA LOCAL OFFSET
CBA MASTER OFFSET


CCB/CDB OFFSET TIMER
$C C C / C D C$ LAG GREEN TIMER
$C C D / C D D$ FORCE OFF TIMER
CCE/CDE IOONG GREEN TIMER
$C C F / C D F$ NO GREEN TIMER


| TIME OF DAY ACTIVITY TABLE |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7+EVENT+HR+MIN+ACT+"E"+ON/OFF+DOW LTS |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | ON/ | S | M | T | W | T | F | 5 |
|  | HR | MIN | ACT | OFE | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 0 | 06 | 00 | 2 | ON/ |  | 2 | 3 | 4 | 5 | 6 |  |
| 1 | 08 | 00 | 2 |  |  | 2 | 3 | 4 | 5 | 6 |  |
| 2 | 14 | 00 | 2 | ON/ |  | 2 | 3 | 4 | 5 | 6 |  |
| 3 | 21 | 00 | 2 | - |  | 2 | 3 | 4 | 5 | 6 |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  |  |  | $i$ |  |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |  |  |  |  |  |
| 8 |  |  |  |  |  |  |  |  |  |  |  |
| 9 |  |  |  |  |  |  |  |  |  |  |  |
| A |  |  |  |  |  |  |  |  |  |  |  |
| B |  | 里至 | - 8 | Sat | - $\mathrm{p}^{2}$ | MEA | ysm | $2=6$ | 53 |  |  |
| C |  |  |  |  |  |  |  |  |  |  |  |
| D |  |  |  |  |  |  |  |  |  |  |  |
| E |  |  |  |  |  |  |  |  |  |  |  |
| F |  |  |  |  |  |  |  |  |  |  |  |

1 TYPE OF MAX TERMINATION
2 MAX 2
3 MAA 3
4 COND SERV (1ST SELECT)
5 COND SERV (2ND SELECT;
6 ENERGIZE AUX OUTPUT-RED

TIME OF DAY NAX RECALL (IST SELECT)
A TRAFFIC ACT. MAX 2 OPERATION
B TIME OF DAY MAX RECALL (2ND SELECT)
C YELLOW YIELD COORDINATION
D YELLOW YIELD COORDINATION
E TIME OF DAY FREE OPERATION
F FLASHING OPERATION
ENERGIZE AUX OUTPUT-GREEN

| CONTROL PLAN TIME OF DAY |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $9+\mathrm{EVENT}+\mathrm{HR}+\mathrm{MIN}+\mathrm{CP}+\mathrm{OS}+\mathrm{E}+\mathrm{DOW}$ |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  | S |  | M | T | W | T | F | S |
|  | HR | MIN | CP | OS | 1 |  | 2 | 3 | 4 | 5 | 6 | 7 |
| 0 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 |  |  |  |  |  |  |  |  |  |  |  |  |
| 9 |  |  |  |  |  |  |  |  |  |  |  |  |
| A |  |  |  |  |  |  |  |  |  |  |  |  |
| E |  |  |  |  |  |  |  |  |  |  |  |  |
| C |  |  |  |  |  |  |  |  |  |  |  |  |
| D |  |  |  |  |  |  |  |  |  |  |  |  |
| E |  |  |  |  |  |  |  |  |  |  |  |  |
| F |  |  |  |  |  |  |  |  |  |  |  |  |




Signal Length Timing Study

City:
San Diego
Intersection:
Dairy Mart and San Ysidro
Date:
1/28/2020
Day:
Tuesday

7:30 am - 7:45 am

| Cycle | Phase | Duration |
| :---: | :---: | :---: |
| 1 | NL/SL | 0:00:15 |
|  | NT/ST | 0:00:20 |
|  | WT/WL | 0:00:10 |
|  | ET/WT | 0:00:15 |
| 2 | NL/NT | 0:00:10 |
|  | NT/ST | 0:00:25 |
|  | WL/WT | 0:00:25 |
|  | ET/WT | 0:00:25 |
| 3 | NL/SL | 0:00:20 |
|  | NT/ST | 0:00:35 |
|  | WL/WT | 0:00:15 |
|  | ET/WT | 0:00:30 |
| 4 | NL/SL | 0:00:20 |
|  | ST/SL | 0:00:10 |
|  | NT/ST | 0:00:20 |
|  | EL/ET | 0:00:15 |
|  | ET/WT | 0:00:15 |
| 5 | NL/NT | 0:00:15 |
|  | NT/ST | 0:00:25 |
|  | EL/ET | 0:00:15 |
|  | ET/WT | 0:00:20 |
| 6 | NL/SL | 0:00:20 |
|  | ET/WT | 0:00:35 |
|  | EL/ET | 0:00:10 |
|  | ET/WT | 0:00:20 |
| 7 | NL/SL | 0:00:20 |
|  | NT/ST | 0:00:10 |
|  | ET/WT | 0:00:30 |
| 8 | NT/ST | 0:00:35 |
|  | ET/WT | 0:00:30 |
| 9 | NL/SL | 0:00:15 |
|  | NT/ST | 0:01:15 |
| 10 | NL/SL | 0:00:10 |
|  | WL/WT | 0:00:10 |
|  | ET/WT | 0:00:30 |

4:30 pm - 4:45 pm

| Cycle | Phase | Duration |
| :---: | :---: | :---: |
| 1 | EL/WL | 0:00:10 |
|  | WL/WT | 0:00:10 |
|  | ET/WT | 0:00:20 |
|  | NL/SL | 0:00:15 |
|  | NT/ST | 0:01:20 |
| 2 | EL/WL | 0:00:15 |
|  | WT/WL | 0:00:25 |
|  | ET/WT | 0:00:25 |
|  | NL/SL | 0:00:25 |
|  | NT/ST | 0:01:25 |
| 3 | WL/WT | 0:00:30 |
|  | ET/WT | 0:00:20 |
|  | NL/SL | 0:00:15 |
|  | NT/ST | 0:00:55 |
| 4 | WL/WT | 0:00:20 |
|  | ET/WT | 0:00:20 |
|  | NT/ST | 0:00:20 |
| 5 | EL/WL | 0:00:15 |
|  | ET/WT | 0:00:30 |
|  | NL/NT | 0:00:20 |
|  | NT/ST | 0:00:30 |
| 6 | EL/WL | 0:00:15 |
|  | ET/WT | 0:00:35 |
|  | NL/SL | 0:00:15 |
|  | NT/ST | 0:00:45 |
| 7 | WL/WT | 0:00:25 |
|  | ET/WT | 0:00:30 |
|  | NL/SL | 0:00:25 |
|  | NT/ST | 0:01:05 |
| 8 | EL/WL | 0:00:10 |
|  | ET/WT | 0:00:30 |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |


| 11 | $\mathrm{NL} / \mathrm{SL}$ | $0: 00: 15$ |
| :---: | :---: | :---: |
|  | $\mathrm{NT} / \mathrm{ST}$ | $0: 00: 25$ |
|  | $\mathrm{EL} / \mathrm{ET}$ | $0: 00: 15$ |
|  | $\mathrm{ET} / \mathrm{WT}$ | $0: 00: 20$ |
| 12 | $\mathrm{NL} / \mathrm{NT}$ | $0: 00: 15$ |
|  | $\mathrm{NT} / \mathrm{ST}$ | $0: 00: 10$ |
|  | $\mathrm{WL} / \mathrm{WT}$ | $0: 00: 15$ |
|  | $\mathrm{ET} / \mathrm{WT}$ | $0: 00: 15$ |
| 13 | $\mathrm{NL} / \mathrm{NT}$ | $0: 00: 10$ |
|  | $\mathrm{NT} / \mathrm{ST}$ | $0: 00: 40$ |

Prepared by AimTD LLC
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714.253.7888


Signal Length Timing Study


Signal Length Timing Study

City:
San Diego
Intersection:
I-5 NB Ramps and San Ysidro
Date:
1/28/2020
Day:
Tuesday

7:30 am - 7:45 am

| Cycle | Phase | Duration |
| :---: | :---: | :---: |
| 1 | ET/WT | 0:01:00 |
|  | NL/NR | 0:00:10 |
|  | WT/WL | 0:00:35 |
| 2 | ET/WT | 0:00:30 |
|  | NL/NR | 0:00:20 |
|  | WT/WL | 0:00:30 |
| 3 | ET/WT | 0:00:50 |
|  | NL/NR | 0:00:20 |
|  | WT/WL | 0:00:20 |
| 4 | ET/WT | 0:00:50 |
|  | NL/NR | 0:00:10 |
|  | WT/WL | 0:00:20 |
| 5 | ET/WT | 0:00:30 |
|  | WT/WL | 0:00:30 |
| 6 | ET/WT | 0:00:35 |
|  | NL/NR | 0:00:10 |
|  | WT/WL | 0:00:35 |
| 7 | ET/WT | 0:00:35 |
|  | NL/NR | 0:00:10 |
|  | WT/WL | 0:00:25 |
| 8 | ET/WT | 0:00:45 |
|  | NL/NR | 0:00:15 |
|  | WT/WL | 0:00:25 |
| 9 | ET/WT | 0:00:35 |
|  | NL/NR | 0:00:10 |
|  | WT/WL | 0:00:30 |
| 10 | ET/WT | 0:00:40 |
|  | NL/NR | 0:00:15 |
|  | WT/WL | 0:00:15 |
| 11 | ET/WT | 0:00:45 |
|  | NL/NR | 0:00:10 |
|  | WT/WL | 0:00:30 |
| 12 | ET/WT | 0:00:45 |
|  |  |  |
|  |  |  |

5:00 pm - 5:15 pm
0:01:45

0:01:20

0:01:30

0:01:20

0:01:00
0:01:20

0:01:10

0:01:25

0:01:15

0:01:10

0:01:25

0:00:45

| Cycle | Phase | Duration |
| :---: | :---: | :---: |
| 1 | WT/WL | 0:00:20 |
|  | ET/WT | 0:00:45 |
|  | NL/NR | 0:00:15 |
| 2 | WT/WL | 0:00:20 |
|  | ET/WT | 0:00:55 |
|  | NL/NR | 0:00:15 |
| 3 | WT/WL | 0:00:25 |
|  | ET/WT | 0:00:35 |
|  | NL/NR | 0:00:15 |
| 4 | WT/WL | 0:00:25 |
|  | ET/WT | 0:00:20 |
|  | NL/NR | 0:00:15 |
| 5 | WT/WL | 0:00:10 |
|  | ET/WT | 0:00:45 |
| 6 | WT/WL | 0:00:20 |
|  | ET/WL | 0:00:30 |
| 7 | WT/WL | 0:00:15 |
|  | ET/WT | 0:00:35 |
|  | NL/NR | 0:00:10 |
| 8 | WT/WL | 0:00:30 |
|  | ET/WT | 0:00:45 |
| 9 | WT/WL | 0:00:25 |
|  | ET/WT | 0:00:40 |
|  | NL/NR | 0:00:15 |
| 10 | WT/WL | 0:00:20 |
|  | ET/WT | 0:00:25 |
|  | NL/NR | 0:00:15 |
| 11 | WT/WL | 0:00:15 |
|  | ET/WT | 0:00:30 |
| 12 | WT/WL | 0:00:20 |
|  | ET/WT | 0:00:30 |
|  | NL/NR | 0:00:15 |
| 13 | WT/WL | 0:00:15 |
|  | ET/WT | 0:00:45 |
|  | NL/NR | 0:00:15 |


|  |  |  | $\begin{gathered} \text { avg } \\ \text { 0:01:17 } \end{gathered}$ | 14 | WT/WL | 0:00:25 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |

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Signal Length Timing Study

City:

Intersection:
Date:
Day:

San Diego
Hollister and Tocayo
1/28/2020
Tuesday

7:00 am - 7:15 am

| Cycle | Phase | Duration |
| :---: | :---: | :---: |
| 1 | ET/WT | 0:01:15 |
|  | ST/SL | 0:00:35 |
|  | NT/ST | 0:00:55 |
|  | EL/WL | 0:00:25 |
| 2 | ET/WT | 0:00:55 |
|  | ST/SL | 0:00:40 |
|  | NT/ST | 0:00:35 |
|  | EL/WL | 0:00:25 |
|  | EL/ET | 0:00:15 |
| 3 | ET/WT | 0:00:50 |
|  | ST/SL | 0:00:35 |
|  | NT/ST | 0:00:35 |
|  | EL/WL | 0:00:15 |
| 4 | ET/WT | 0:00:35 |
|  | ST/SL | 0:00:50 |
|  | NT/ST | 0:00:35 |
| 5 | EL/WL | 0:00:15 |
|  | ST/SL | 0:00:40 |
|  | NT/ST | 0:00:15 |
| 6 | ET/WT | 0:00:20 |
|  | ST/SL | 0:00:40 |
|  | NT/ST | 0:00:20 |
|  | ET/EL | 0:00:15 |
| 7 | ET/WT | 0:00:25 |
|  | ST/SL | 0:00:35 |
|  | NT/ST | 0:00:35 |
|  | EL/WL | 0:00:15 |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |

4:00 pm - 4:15 pm

| Cycle | Phase | Duration |
| :---: | :---: | :---: |
| 1 | NL/SL | 0:00:20 |
|  | NT/ST | 0:00:15 |
|  | ET/WT | 0:00:15 |
| 2 | ST/SL | 0:00:45 |
|  | NT/ST | 0:00:30 |
|  | WT/WL | 0:00:15 |
|  | ET/EL | 0:00:15 |
| 3 | NL/SL | 0:00:45 |
|  | NT/ST | 0:00:15 |
|  | WT/WL | 0:00:20 |
|  | ET/EL | 0:00:30 |
| 4 | NL/SL | 0:00:35 |
|  | NT/ST | 0:00:15 |
|  | EL/WL | 0:00:10 |
|  | ET/WT | 0:00:25 |
| 5 | NL/SL | 0:00:40 |
|  | ST/SL | 0:00:25 |
|  | EL/WL | 0:00:25 |
| 6 | NL/SL | 0:00:10 |
|  | NT/NL | 0:00:25 |
| 7 | NL/SL | 0:00:10 |
|  | ST/SL | 0:00:30 |
|  | ET/WT | 0:00:25 |
| 8 | NL/SL | 0:00:20 |
|  | NL/NT | 0:00:15 |
| 9 | NL/SL | 0:00:35 |
|  | WT/WL | 0:00:20 |
|  | ET/EL | 0:00:15 |
| 10 | NL/SL | 0:00:20 |
|  | NT/ST | 0:00:45 |
|  | WT/WL | 0:00:20 |
|  | ET/WT | 0:00:15 |
| 11 | NL/SL | 0:00:25 |
|  | NT/NL | 0:00:15 |
|  | NT/ST | 0:00:30 |


|  |  |  |
| :--- | :--- | :--- |
|  |  |  |
|  |  |  |


|  | $\mathrm{EL} / \mathrm{WL}$ | $0: 00: 10$ |
| :--- | :--- | :--- |
| 12 | $\mathrm{NL} / \mathrm{SL}$ | $0: 00: 55$ |
|  | $\mathrm{ST} / \mathrm{SL}$ | $0: 00: 20$ |

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## APPENDIX B

Data from CDPR - Goat Canyon Sediment Management Site

| Date | Haul Total (cy) | Invoice \# | \# Truck Trips | Truck Type | Project Location | Customer |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 11/7/2016 | 320 | 139 | 8 | *(8) 40 cy roll off container | Missing Daily Spreadsheets for roll-off containers |  |
| 10/29/2016 | 11,408 |  | 368 |  |  |  |
| 10/14/2016 | 3,596 |  | 116 | 637 Cat Scraper (2 scrappers, on an average 58 loads per day) | Border Field State Park | State Parks |
| 10/17/2016 | 2,666 |  | 86 | 637 Cat Scraper (2 scrappers, on an average 43 loads per day) | Border Field State Park | State Parks |
| 10/18/2016 | 1,116 |  | 36 | 637 Cat Scraper (2 scrappers, on an average 17 loads per day) | Border Field State Park | State Parks |
| 10/19/2016 | 4,030 |  | 130 | 637 Cat Scraper (2 scrappers, on an average 65 loads per day) | Border Field State Park | State Parks |
|  |  |  |  |  |  |  |
| 3/7/2017 | 2314 | 151 | 172 |  | Missing Daily Spreadsheets |  |
|  |  |  |  |  |  |  |
| 3/7/2017 | 80 | 151 | 2 | *(2) 40 cy roll off container | Missing Daily Spreadsheets |  |
|  |  |  |  |  |  |  |
| 4/15/2017 | 2236 | 155 | 172 |  |  |  |
| 3/4/2017 | 104 |  | 8 | export, super tens (1 truck) | Border Field Park | Hofer |
| 3/8/2017 | 208 |  | 16 | export super tens(2 trucks, 8 loads each) | Border Field Park | Hofer |
| 3/9/2017 | 208 |  | 16 | export super tens(2 trucks, 8 loads each) | Border Field Park | Hofer |
| 4/10/2017 | 1105 |  | 85 | export, super tens, (11 trucks, on an average 6-8 loads each) | Border Patrol | Otay Mesa |
| 4/11/2017 | 611 |  | 47 | export, super tens, (10 trucks, on an average 4-5 loads each) | Border Patrol | Otay Mesa |
|  |  | Avg | 34 |  |  |  |
|  |  |  |  |  |  |  |
| 4/29/2017 | 4710 | 156 | 314 |  |  |  |
| 4/24/2017 | 1155 |  | 77 | bottom dumps, (14 trucks, on an average 6-7 loads per day) | Otay Mesa | Caltrans |
| 4/25/2017 | 990 |  | 66 | bottom dumps, (11 trucks, on an average 6 loads per day) |  | Caltrans |
| 4/26/2017 | 1155 |  | 77 | bottom dumps, (11 trucks, on an average 7 loads per day) | Otay Mesa | Caltrans |
| 4/27/2017 | 1410 |  | 94 | bottom dumps, (15 trucks, on an average 6-7 loads per day) | Otay Mesa | Caltrans |
|  |  | Avg | 79 |  |  |  |
|  |  |  |  |  |  |  |
| 5/13/2017 | 5919 | 157 | 443 |  |  |  |
| 5/1/2017 | 780 |  | 60 | super tens, (10 trucks, on an average 6 loads per day) | Otay Mesa | Cerrudo |
| 5/2/2017 | 1092 |  | 84 | super tens, (11 trucks, on an average 6-8 loads per day) | Otay Mesa | Cerrudo |
| 5/3/2017 | 1144 |  | 88 | super tens, (11 trucks, on an average 8 loads per day) | Otay Mesa | Cerrudo |
| 5/4/2017 | 182 |  | 14 | super tens, (2 trucks, on an average 7 loads per day) | Otay Mesa | Cerrudo |
| 5/9/2017 | 1014 |  | 78 | super tens, (12 trucks, on an average 6-7 loads per day) | Otay Mesa | Cerrudo |
| 5/11/2017 | 1200 |  | 80 | super tens, (10 trucks, on an average 8 loads per day) | Otay Mesa | Cerrudo |
| 5/12/2017 | 507 |  | 39 | super tens, (6 trucks, on an average 6-7 loads per day) |  |  |
|  |  | Avg | 63 |  |  |  |
|  |  |  |  |  |  |  |
| 5/22/2017-6/18/2017 | 2175 | 158 | 145 | export, bottom dumps (17 trucks, on an average 7-10 loads per day) | Terra Bella Nursery, Chula Vista | Western |
| 6/18/2017 | 400 | 158 | 10 | *(10) 40 cy roll off container |  |  |
| 6/18/2017 | 360 | 158 | 9 | *(9) 40 cy roll off container |  |  |
|  |  |  |  |  |  |  |
| 7/27/2017 | 4895 | 161 | 361 |  | Hofer Facility, Chula Vista |  |
|  | 1515 |  | 101 | export, bottom dumps 15 cy (10 trucks, on an average 9-10 truck loads ) | Airway Rd |  |
|  | 1716 |  | 132 | super tens ( 13 cy ) ( 15 trucks, 8-9 per day) | Border Field State Park |  |
|  | 1664 |  | 128 | export, super tens (14 trucks, 9-10 loads per day) |  |  |
|  |  | Avg | 120 |  |  |  |
|  |  |  |  |  |  |  |
| 7/27/2017 | 160 | 161 | 4 | *(4) 40 cy roll off container of matrial from lower basin and removed off-site. |  |  |
| 8/20/2017 | 1586 | 165 | 122 | export, super tens (12 trucks, 10-11 loads per day) | From Goat Canyon to Hofer Facility |  |
| 8/11/2017 |  |  | 178 | (2 trucks, every 5 minutes) | Border Field State Park |  |
| 8/14/2017 |  |  | 88 | (2 trucks, every 5 minutes) | Border Field State Park |  |
| 8/15/2017 |  |  | 123 | (2 trucks, every 5 minutes) | Border Field State Park |  |


| Date | Invoice \# | Haul Total (cy) | \# Truck Trips | Truck Type | Project Location | Customer | Truck Volume/load (cy) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10/1/2017 | 170 | 41984 | 1388 |  |  |  |  |
| 8/15/2017 |  | 3434 | 123 | (2 trucks, 60-63 loads per day) | Border Field |  | 31 |
| 8/16/2017 |  | 3434 | 136 | (2 trucks, 63-73 loads per day) | Border Field |  | 31 |
| 8/17/2017 |  | 4030 | 130 | (2trucks, 65 loads per day) | Border Field |  | 31 |
| 8/18/2017 |  | 4712 | 152 | (2 trucks, $74-78$ loads per day) | Border Field |  | 31 |
| 8/21/2017 |  | 4526 | 146 | (2 trucks, 73 loads per day) | Border Field |  | 31 |
| 8/25/2017 |  | 3937 | 127 | (2 trucks, 61-66 loads per day) | Border Field |  | 31 |
| 8/28/2017 |  | 4185 | 135 | (2 trucks, 66-67 loads per day) | Border Field |  | 31 |
| 8/29/2017 |  | 4557 | 147 | (2 trucks, $73-74$ loads per day) | Border Field |  | 31 |
| 8/30/2017 |  | 4154 | 134 | (2 trucks, 67 loads per day) | Border Field |  | 31 |
| 8/31/2017 |  | 4495 | 145 | (2 trucks, 72-73 loads per day) | Border Field |  | 31 |
|  |  | 520 | 13 | 40 CY Roll-Off Containers |  |  | 40 |



| 4/26/2018 | 189 | 3930 | 262 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4/20/2018 |  | 1830 | 122 | bottom dumps (10 trucks, 12-13 loads per day) | Terra Bella Nursery | 15 |
| 4/21/2018 |  | 2100 | 140 | bottom dumps (12 trucks, 10-12 loads per day) | Terra Bella Nursery | 15 |





## - Existing Conditions



## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 4 | 7 | \% | 4 | $\stackrel{7}{ }$ | \% | 4 | 7 | ${ }^{7}$ | 4 | 7 |
| Traffic Volume (veh/h) 29 | 267 | 60 | 49 | 112 | 157 | 129 | 159 | 538 | 188 | 78 | 52 |
| Future Volume (veh/h) 29 | 267 | 60 | 49 | 112 | 157 | 129 | 159 | 538 | 188 | 78 | 52 |
| Initial Q $(Q b)$, veh 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) 1.00 |  | 0.98 | 1.00 |  | 0.98 | 0.99 |  | 0.99 | 1.00 |  | 1.00 |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 |
| Adj Flow Rate, veh/h 34 | 310 | 70 | 57 | 130 | 183 | 150 | 185 | 626 | 219 | 91 | 0 |
| Peak Hour Factor 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Percent Heavy Veh, \% 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h 63 | 408 | 339 | 88 | 434 | 359 | 687 | 635 | 610 | 483 | 687 |  |
| Arrive On Green 0.04 | 0.22 | 0.22 | 0.05 | 0.23 | 0.23 | 0.08 | 0.34 | 0.34 | 0.11 | 0.37 | 0.00 |
| Sat Flow, veh/h 1767 | 1856 | 1544 | 1767 | 1856 | 1536 | 1767 | 1856 | 1554 | 1767 | 1856 | 1572 |
| Grp Volume(v), veh/h 34 | 310 | 70 | 57 | 130 | 183 | 150 | 185 | 626 | 219 | 91 | 0 |
| Grp Sat Flow(s),veh/h/ln1767 | 1856 | 1544 | 1767 | 1856 | 1536 | 1767 | 1856 | 1554 | 1767 | 1856 | 1572 |
| Q Serve(g_s), s 1.2 | 10.1 | 2.4 | 2.0 | 3.7 | 6.7 | 3.4 | 4.7 | 22.0 | 5.0 | 2.1 | 0.0 |
| Cycle Q Clear(g_c), s 1.2 | 10.1 | 2.4 | 2.0 | 3.7 | 6.7 | 3.4 | 4.7 | 22.0 | 5.0 | 2.1 | 0.0 |
| Prop In Lane 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h 63 | 408 | 339 | 88 | 434 | 359 | 687 | 635 | 610 | 483 | 687 |  |
| V/C Ratio(X) 0.54 | 0.76 | 0.21 | 0.65 | 0.30 | 0.51 | 0.22 | 0.29 | 1.03 | 0.45 | 0.13 |  |
| Avail Cap(c_a), veh/h 247 | 635 | 528 | 247 | 635 | 526 | 792 | 635 | 610 | 538 | 687 |  |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh 30.5 | 23.5 | 20.5 | 30.0 | 20.3 | 21.4 | 11.7 | 15.5 | 19.6 | 11.3 | 13.4 | 0.0 |
| Incr Delay (d2), s/veh 7.2 | 2.9 | 0.3 | 7.8 | 0.4 | 1.1 | 0.2 | 1.2 | 43.4 | 0.7 | 0.4 | 0.0 |
| Initial Q Delay(d3),s/veh 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/lm0. 6 | 4.4 | 0.8 | 1.0 | 1.6 | 0.1 | 1.2 | 2.0 | 15.3 | 1.8 | 0.9 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh 37.7 | 26.4 | 20.8 | 37.8 | 20.7 | 22.5 | 11.9 | 16.6 | 62.9 | 12.0 | 13.8 | 0.0 |
| LnGrp LOS D | C | C | D | C | C | B | B | F | B | B |  |
| Approach Vol, veh/h | 414 |  |  | 370 |  |  | 961 |  |  | 310 | A |
| Approach Delay, s/veh | 26.4 |  |  | 24.2 |  |  | 46.1 |  |  | 12.5 |  |
| Approach LOS | C |  |  | C |  |  | D |  |  | B |  |


| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), $\$ 1.5$ | 26.5 | 7.7 | 18.6 | 9.7 | 28.3 | 6.8 | 19.5 |  |
| Change Period (Y+Rc), s 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |  |
| Max Green Setting (Gmax9., B | 22.0 | 9.0 | 22.0 | 9.0 | 22.0 | 9.0 | 22.0 |  |
| Max Q Clear Time (g_c+117,, © | 24.0 | 4.0 | 12.1 | 5.4 | 4.1 | 3.2 | 8.7 |  |
| Green Ext Time (p_c), s | 0.1 | 0.0 | 0.0 | 1.5 | 0.1 | 0.4 | 0.0 | 1.1 |

Intersection Summary

| HCM 6th Ctrl Delay | 33.1 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

Unsignalized Delay for [SBR] is excluded from calculations of the approach delay and intersection delay.


## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Intersection |
| :--- |
| Intersection Delay, s/veh 16 |
| Intersection LOS |
| C |


| Movement EBL | EBL | EBR | NBL | NBT | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% |  |  | $\uparrow$ | 44 | 7 |
| Traffic Vol, veh/h 261 | 261 | 20 | 6 | 319 | 179 | 112 |
| Future Vol, veh/h 261 | 261 | 20 | 6 | 319 | 179 | 112 |
| Peak Hour Factor 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow 297 | 297 | 23 | 7 | 363 | 203 | 127 |
| Number of Lanes | 1 | 0 | 0 | 1 | 2 | 1 |
| Approach E | EB |  | NB |  | SB |  |
| Opposing Approach |  |  | SB |  | NB |  |
| Opposing Lanes | 0 |  | 3 |  | 1 |  |
| Conflicting Approach Left S | SB |  | EB |  |  |  |
| Conflicting Lanes Left | 3 |  | 1 |  | 0 |  |
| Conflicting Approach RighN | NB |  |  |  | EB |  |
| Conflicting Lanes Right | 1 |  | 0 |  | 1 |  |
| HCM Control Delay 19 | 19.3 |  | 19.1 |  | 9.2 |  |
| HCM LOS | C |  | C |  | A |  |


| Lane | NBLn1 EBLn1 SBLn1 SBLn2 SBLn3 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $2 \%$ | $93 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $98 \%$ | $0 \%$ | $100 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, \% | $0 \%$ | $7 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 325 | 281 | 90 | 90 | 112 |
| LT Vol | 6 | 261 | 0 | 0 | 0 |
| Through Vol | 319 | 0 | 90 | 90 | 0 |
| RT Vol | 0 | 20 | 0 | 0 | 112 |
| Lane Flow Rate | 369 | 319 | 102 | 102 | 127 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.634 | 0.602 | 0.178 | 0.178 | 0.135 |
| Departure Headway (Hd) | 6.181 | 6.791 | 6.305 | 6.305 | 3.809 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 584 | 530 | 568 | 568 | 933 |
| Service Time | 3.936 | 4.539 | 4.065 | 4.065 | 1.568 |
| HCM Lane V/C Ratio | 0.632 | 0.602 | 0.18 | 0.18 | 0.136 |
| HCM Control Delay | 19.1 | 19.3 | 10.4 | 10.4 | 7.2 |
| HCM Lane LOS | C | C | B | B | A |
| HCM 95th-tile Q | 4.4 | 3.9 | 0.6 | 0.6 | 0.5 |


| Intersection |
| :--- |
| Intersection Delay, s/veh10.2 |
| Intersection LOS B |


| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Configurations | $\boldsymbol{j}$ | $\overrightarrow{\mathbf{F}}$ | $\hat{\mathbf{f}}$ |  |  | $\uparrow$ |
| Traffic Vol, ven/h | 5 | 313 | 16 | 6 | 166 | 25 |
| Future Vol, veh/h | 5 | 313 | 16 | 6 | 166 | 25 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 5 | 344 | 18 | 7 | 182 | 27 |
| Number of Lanes | 1 | 1 | 1 | 0 | 0 | 1 |


| Approach W | NB | SB |
| :---: | :---: | :---: |
| Opposing Approach | SB | NB |
| Opposing Lanes | 1 | 1 |
| Conflicting Approach Left N |  | WB |
| Conflicting Lanes Left | 0 | 2 |
| Conflicting Approach Righis | WB |  |
| Conflicting Lanes Right | 2 | 0 |
| HCM Control Delay 10, | 8.1 | 10 |
| HCM LOS | A | A |


| Lane | NBLn1WBLn1WBLn2 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $100 \%$ | $0 \%$ | $87 \%$ |
| Vol Thru, \% | $73 \%$ | $0 \%$ | $0 \%$ | $13 \%$ |
| Vol Right, \% | $27 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 22 | 5 | 313 | 191 |
| LT Vol | 0 | 5 | 0 | 166 |
| Through Vol | 16 | 0 | 0 | 25 |
| RT Vol | 6 | 0 | 313 | 0 |
| Lane Flow Rate | 24 | 5 | 344 | 210 |
| Geometry Grp | 2 | 7 | 7 | 2 |
| Degree of Util (X) | 0.033 | 0.009 | 0.425 | 0.289 |
| Departure Headway (Hd) | 4.868 | 5.652 | 4.446 | 4.958 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 732 | 634 | 808 | 724 |
| Service Time | 2.921 | 3.379 | 2.173 | 2.998 |
| HCM Lane V/C Ratio | 0.033 | 0.008 | 0.426 | 0.29 |
| HCM Control Delay | 8.1 | 8.4 | 10.4 | 10 |
| HCM Lane LOS | A | A | B | A |
| HCM 95th-tile Q | 0.1 | 0 | 2.1 | 1.2 |

6: Clearwater Way \& Dairy Mart Rd

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.6 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\hat{7}$ |  | 1 | a | r |  |
| Traffic Vol, veh/h | 19 | 6 | 12 | 32 | 7 | 8 |
| Future Vol, veh/h | 19 | 6 | 12 | 32 | 7 | 8 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 235 | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 79 | 79 | 79 | 79 | 79 | 79 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 24 | 8 | 15 | 41 | 9 | 10 |


| Major/Minor M | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 32 | 0 | 99 | 28 |
| Stage 1 | - | - | - | - | 28 | - |
| Stage 2 | - | - | - | - | 71 | - |
| Critical Hdwy | - | - | 4.13 | - | 6.43 | 6.23 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.43 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.43 | - |
| Follow-up Hdwy | - | - | 2.227 | - | 3.527 | 3.327 |
| Pot Cap-1 Maneuver | - | - | 1574 | - | 897 | 1044 |
| Stage 1 | - | - | - | - | 992 | - |
| Stage 2 | - | - | - | - | 949 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1574 | - | 888 | 1044 |
| Mov Cap-2 Maneuver | - | - | - | - | 888 | - |
| Stage 1 | - | - | - | - | 992 | - |
| Stage 2 | - | - | - | - | 940 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 2 |  | 8.8 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 EBT EBR WBL WBT |  |  |  |  |
| Capacity (veh/h) |  | 965 | - | - | 1574 | - |
| HCM Lane V/C Ratio |  | 0.02 | - | - | 0.01 | - |
| HCM Control Delay (s) |  | 8.8 | - | - | 7.3 | - |
| HCM Lane LOS |  | A | - | - | A | - |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.7 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\hat{7}$ |  |  | - | F |  |
| Traffic Vol, veh/h | 11 | 0 | 18 | 17 | 2 | 6 |
| Future Vol, veh/h | 11 | 0 | 18 | 17 | 2 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 61 | 61 | 61 | 61 | 61 | 61 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 18 | 0 | 30 | 28 | 3 | 10 |


| Major/Minor | Major1 | Major2 |  |  | Minor1 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Conflicting Flow All | 0 | 0 | 18 | 0 | 106 | 18 |  |
| $\quad$ Stage 1 | - | - | - | - | 18 | - |  |
| Stage 2 | - | - | - | - | 88 | - |  |
| Critical Hdwy | - | - | 4.13 | - | 6.43 | 6.23 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.43 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.43 | - |  |
| Follow-up Hdwy | - | - | 2.227 | -3.527 | 3.327 |  |  |
| Pot Cap-1 Maneuver | - | - | 1592 | - | 889 | 1058 |  |
| Stage 1 | - | - | - | - | 1002 | - |  |
| Stage 2 | - | - | - | - | 933 | - |  |
| Platoon blocked, \% | - | - |  | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | 1592 | - | 872 | 1058 |  |
| Mov Cap-2 Maneuver | - | - | - | - | 872 | - |  |
| Stage 1 | - | - | - | -1002 | - |  |  |
| Stage 2 | - | - | - | - | 915 | - |  |


| Approach | EB | WB | NB |
| :--- | ---: | :---: | :---: |
| HCM Control Delay, s | 0 | 3.8 | 8.6 |

HCM LOS A

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1004 | - | - | 1592 | - |
| HCM Lane V/C Ratio | 0.013 | - | -0.019 | - |  |
| HCM Control Delay (s) | 8.6 | - | - | 7.3 | 0 |
| HCM Lane LOS | A | - | - | A | A |
| HCM 95th \%tile Q(veh) | 0 | - | - | 0.1 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 4.9 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | -1 | 1 |  | M |  |
| Traffic Vol, veh/h | 6 | 3 | 3 | 5 | 6 | 5 |
| Future Vol, veh/h | 6 | 3 | 3 | 5 | 6 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 88 | 88 | 88 | 88 | 88 | 88 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 7 | 3 | 3 | 6 | 7 | 6 |


| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | ---: | :--- | :--- | :--- | ---: | ---: |
| Conflicting Flow All | 9 | 0 | - | 0 | 23 | 6 |
| $\quad$ Stage 1 | - | - | - | - | 6 | - |
| $\quad$ Stage 2 | - | - | - | - | 17 | - |
| Critical Hdwy | 4.13 | - | - | - | 6.43 | 6.23 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.43 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.43 | - |
| Follow-up Hdwy | 2.227 | - | - | -3.527 | 3.327 |  |
| Pot Cap-1 Maneuver | 1604 | - | - | - | 991 | 1074 |
| $\quad$ Stage 1 | - | - | - | - | 1014 | - |
| Stage 2 | - | - | - | - | 1003 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1604 | - | - | - | 987 | 1074 |
| Mov Cap-2 Maneuver | - | - | - | - | 987 | - |
| Stage 1 | - | - | - | - | 1010 | - |
| Stage 2 | - | - | - | - | 1003 | - |


| Approach | EB | WB | SB |
| :--- | :--- | ---: | :--- |
| HCM Control Delay, s | 4.8 | 0 | 8.6 |

HCM LOS A

| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1604 | - | - | -1025 |
| HCM Lane V/C Ratio | 0.004 | - | - | -0.012 |
| HCM Control Delay (s) | 7.3 | 0 | - | - |
| HCM Lane LOS | A | A | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | - | - |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | 个 $\uparrow$ |  | \％ | 个隹 |  | ${ }^{7}$ | $\hat{}$ |  | 7 | $\hat{\beta}$ |  |
| Traffic Volume（veh／h） | 32 | 49 | 2 | 48 | 24 | 540 | 0 | 71 | 96 | 455 | 56 | 21 |
| Future Volume（veh／h） | 32 | 49 | 2 | 48 | 24 | 540 | 0 | 71 | 96 | 455 | 56 | 21 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 0.99 | 1.00 |  | 0.99 | 1.00 |  | 0.97 | 1.00 |  | 0.98 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 |
| Adj Flow Rate，veh／h | 40 | 60 | 2 | 59 | 30 | 667 | 0 | 88 | 119 | 562 | 69 | 26 |
| Peak Hour Factor | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 |
| Percent Heavy Veh，\％ | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap，veh／h | 58 | 1030 | 34 | 77 | 540 | 477 | 2 | 216 | 291 | 322 | 678 | 256 |
| Arrive On Green | 0.03 | 0.30 | 0.30 | 0.04 | 0.31 | 0.31 | 0.00 | 0.31 | 0.31 | 0.18 | 0.53 | 0.53 |
| Sat Flow，veh／h | 1767 | 3481 | 115 | 1767 | 1763 | 1557 | 1767 | 703 | 951 | 1767 | 1276 | 481 |
| Grp Volume（v），veh／h | 40 | 30 | 32 | 59 | 30 | 667 | 0 | 0 | 207 | 562 | 0 | 95 |
| Grp Sat Flow（s），veh／h／n | 1767 | 1763 | 1833 | 1767 | 1763 | 1557 | 1767 | 0 | 1655 | 1767 | 0 | 1757 |
| Q Serve（g＿s），s | 2.3 | 1.3 | 1.3 | 3.5 | 1.3 | 32.0 | 0.0 | 0.0 | 10.4 | 19.0 | 0.0 | 2.8 |
| Cycle Q Clear（g＿c），s | 2.3 | 1.3 | 1.3 | 3.5 | 1.3 | 32.0 | 0.0 | 0.0 | 10.4 | 19.0 | 0.0 | 2.8 |
| Prop In Lane | 1.00 |  | 0.06 | 1.00 |  | 1.00 | 1.00 |  | 0.57 | 1.00 |  | 0.27 |
| Lane Grp Cap（c），veh／h | 58 | 522 | 542 | 77 | 540 | 477 | 2 | 0 | 507 | 322 | 0 | 934 |
| V／C Ratio（X） | 0.69 | 0.06 | 0.06 | 0.77 | 0.06 | 1.40 | 0.00 | 0.00 | 0.41 | 1.75 | 0.00 | 0.10 |
| Avail Cap（c＿a），veh／h | 322 | 540 | 562 | 322 | 540 | 477 | 322 | 0 | 507 | 322 | 0 | 934 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（1） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 50.0 | 26.3 | 26.3 | 49.4 | 25.6 | 36.2 | 0.0 | 0.0 | 28.7 | 42.7 | 0.0 | 12.1 |
| Incr Delay（d2），s／veh | 13.5 | 0.0 | 0.0 | 14.8 | 0.0 | 191.5 | 0.0 | 0.0 | 2.4 | 349.2 | 0.0 | 0.2 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（ $50 \%$ ），veh／ln | 1.3 | 0.6 | 0.6 | 1.8 | 0.5 | 37.1 | 0.0 | 0.0 | 4.4 | 39.4 | 0.0 | 1.1 |

Unsig．Movement Delay，s／veh

| LnGrp Delay（d），s／veh | 63.5 | 26.4 | 26.4 | 64.2 | 25.6 | 227.7 | 0.0 | 0.0 | 31.1 | 391.9 | 0.0 | 12.3 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LnGrp LOS | E | C | C | E | C | F | A | A | C | F | A | B |
| Approach Vol，veh／h |  | 102 |  |  | 756 |  |  | 207 |  | 657 |  |  |
| Approach Delay，s／veh |  | 40.9 |  |  | 206.9 |  |  | 31.1 |  | 337.0 |  |  |
| Approach LOS | D |  |  | F |  |  | C |  | F |  |  |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 23.5 | 36.5 | 9.0 | 35.4 | 0.0 | 60.0 | 7.9 | 36.5 |
| Change Period（Y＋Rc），s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting（Gmax），s | 19.0 | 32.0 | 19.0 | 32.0 | 19.0 | 32.0 | 19.0 | 32.0 |
| Max Q Clear Time（g＿c＋11），s | 21.0 | 12.4 | 5.5 | 3.3 | 0.0 | 4.8 | 4.3 | 34.0 |
| Green Ext Time（p＿c），s | 0.0 | 1.2 | 0.1 | 0.3 | 0.0 | 0.5 | 0.0 | 0.0 |

Intersection Summary

| HCM 6th Ctrl Delay | 225.6 |
| :--- | ---: |
| HCM 6th LOS | F |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Y |  | $\hat{i}$ |  |  | - |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 0 | 0 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 0 | 0 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1 | 0 | 0 | 0 | 0 | 0 |
| Stage 1 | 0 | - | - | - | - | - |
| Stage 2 | 1 | - | - | - | - | - |
| Critical Hdwy | 6.43 | 6.23 | - | - | 4.13 | - |
| Critical Hdwy Stg 1 | 5.43 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.43 | - | - | - | - | - |
| Follow-up Hdwy | 3.527 | 3.327 | - | - | 2.227 | - |
| Pot Cap-1 Maneuver | 1019 | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | 1020 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 1019 | - | - | - | - | - |
| Mov Cap-2 Maneuver | 1019 | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | 1020 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 0 |  | 0 |  | 0 |  |
| HCM LOS | A |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | - | - | - |
| HCM Lane V/C Ratio |  | - | - | - | - | - |
| HCM Control Delay (s) |  | - | - | 0 | 0 | - |
| HCM Lane LOS |  | - | - | A | A | - |
| HCM 95th \%tile Q(veh) |  | - | - | - | - | - |



## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 4 | F | \% | 4 | I' | * | 4 | 7 | * | 4 | 7 |
| Traffic Volume (veh/h) 26 | 176 | 110 | 152 | 101 | 150 | 150 | 210 | 654 | 206 | 203 | 57 |
| Future Volume (veh/h) 26 | 176 | 110 | 152 | 101 | 150 | 150 | 210 | 654 | 206 | 203 | 57 |
| Initial Q $(Q b)$, veh 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) 1.00 |  | 0.94 | 1.00 |  | 0.97 | 0.99 |  | 0.96 | 0.99 |  | 1.00 |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 |
| Adj Flow Rate, veh/h 27 | 183 | 115 | 158 | 105 | 156 | 156 | 219 | 681 | 215 | 211 | 0 |
| Peak Hour Factor 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh, \% 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h 51 | 309 | 247 | 203 | 470 | 384 | 607 | 702 | 752 | 456 | 747 |  |
| Arrive On Green 0.03 | 0.17 | 0.17 | 0.11 | 0.25 | 0.25 | 0.08 | 0.38 | 0.38 | 0.10 | 0.40 | 0.00 |
| Sat Flow, veh/h 1767 | 1856 | 1483 | 1767 | 1856 | 1518 | 1767 | 1856 | 1509 | 1767 | 1856 | 1572 |
| Grp Volume(v), veh/h 27 | 183 | 115 | 158 | 105 | 156 | 156 | 219 | 681 | 215 | 211 | 0 |
| Grp Sat Flow(s),veh/h/ln1767 | 1856 | 1483 | 1767 | 1856 | 1518 | 1767 | 1856 | 1509 | 1767 | 1856 | 1572 |
| Q Serve(g_s), s 1.1 | 6.9 | 5.3 | 6.6 | 3.4 | 6.5 | 4.0 | 6.3 | 28.7 | 5.4 | 5.8 | 0.0 |
| Cycle Q Clear(g_c), s 1.1 | 6.9 | 5.3 | 6.6 | 3.4 | 6.5 | 4.0 | 6.3 | 28.7 | 5.4 | 5.8 | 0.0 |
| Prop In Lane 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h 51 | 309 | 247 | 203 | 470 | 384 | 607 | 702 | 752 | 456 | 747 |  |
| V/C Ratio(X) 0.53 | 0.59 | 0.47 | 0.78 | 0.22 | 0.41 | 0.26 | 0.31 | 0.91 | 0.47 | 0.28 |  |
| Avail Cap(c_a), veh/h 142 | 478 | 382 | 968 | 1345 | 1100 | 714 | 702 | 752 | 637 | 747 |  |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh 36.3 | 29.2 | 28.5 | 32.6 | 22.4 | 23.5 | 12.4 | 16.6 | 17.7 | 12.0 | 15.2 | 0.0 |
| Incr Delay (d2), s/veh 8.5 | 1.8 | 1.4 | 6.3 | 0.2 | 0.7 | 0.2 | 1.2 | 16.5 | 0.8 | 0.9 | 0.0 |
| Initial Q Delay(d3), s/veh 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/lm0. 6 | 3.1 | 1.9 | 3.1 | 1.5 | 0.1 | 1.5 | 2.8 | 13.1 | 2.1 | 2.5 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh 44.8 | 31.0 | 29.9 | 38.9 | 22.6 | 24.2 | 12.6 | 17.7 | 34.2 | 12.8 | 16.2 | 0.0 |
| LnGrp LOS D | C | C | D | C | C | B | B | C | B | B |  |
| Approach Vol, veh/h | 325 |  |  | 419 |  |  | 1056 |  |  | 426 | A |
| Approach Delay, s/veh | 31.7 |  |  | 29.4 |  |  | 27.6 |  |  | 14.5 |  |
| Approach LOS | C |  |  | C |  |  | C |  |  | B |  |


| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), $\$ 2.2$ | 33.2 | 13.2 | 17.1 | 10.4 | 35.0 | 6.7 | 23.7 |  |
| Change Period (Y+Rc), s 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |  |
| Max Green Setting (Gmaxp. 5 | 25.5 | 41.5 | 19.5 | 10.5 | 30.5 | 6.1 | 54.9 |  |
| Max Q Clear Time (g_c+117, $\mathbf{s}$ | 30.7 | 8.6 | 8.9 | 6.0 | 7.8 | 3.1 | 8.5 |  |
| Green Ext Time (p_c), s | 0.4 | 0.0 | 0.4 | 1.0 | 0.2 | 1.1 | 0.0 | 1.2 |

Intersection Summary

| HCM 6th Ctrl Delay | 26.0 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

Unsignalized Delay for [SBR] is excluded from calculations of the approach delay and intersection delay.

| 4 |  |  |  | $\Perp$ |  | 4 | $\dagger$ | $p$ | * | $\frac{1}{*}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 4 | $\stackrel{7}{ }$ |  |  |  |  | 4 | $\underset{ }{7}$ | \% | 4 |  |
| Traffic Volume (veh/h) 548 | 1 | 456 | 0 | 0 | 0 | 0 | 470 | 43 | 188 | 277 | 0 |
| Future Volume (veh/h) 548 | 1 | 456 | 0 | 0 | 0 | 0 | 470 | 43 | 188 | 277 | 0 |
| Initial Q (Qb), veh 0 | 0 | 0 |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) 1.00 |  | 1.00 |  |  |  | 1.00 |  | 0.98 | 1.00 |  | 1.00 |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  |  |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln 1856 | 1856 | 1856 |  |  |  | 0 | 1856 | 1856 | 1856 | 1856 | 0 |
| Adj Flow Rate, veh/h 559 | 1 | 465 |  |  |  | 0 | 480 | 44 | 192 | 283 | 0 |
| Peak Hour Factor 0.98 | 0.98 | 0.98 |  |  |  | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Percent Heavy Veh, \% 3 | 3 | 3 |  |  |  | 0 | 3 | 3 | 3 | 3 | 0 |
| Cap, veh/h 605 | 1 | 539 |  |  |  | 0 | 732 | 608 | 224 | 1047 | 0 |
| Arrive On Green 0.34 | 0.34 | 0.34 |  |  |  | 0.00 | 0.39 | 0.39 | 0.13 | 0.56 | 0.00 |
| Sat Flow, veh/h 1764 | 3 | 1571 |  |  |  | 0 | 1856 | 1540 | 1767 | 1856 | 0 |
| Grp Volume(v), veh/h 560 | 0 | 465 |  |  |  | 0 | 480 | 44 | 192 | 283 | 0 |
| Grp Sat Flow(s),veh/h/ln1767 | 0 | 1571 |  |  |  | 0 | 1856 | 1540 | 1767 | 1856 | 0 |
| Q Serve(g_s), s 33.5 | 0.0 | 30.4 |  |  |  | 0.0 | 23.2 | 2.0 | 11.7 | 8.6 | 0.0 |
| Cycle Q Clear(g_c), s 33.5 | 0.0 | 30.4 |  |  |  | 0.0 | 23.2 | 2.0 | 11.7 | 8.6 | 0.0 |
| Prop In Lane 1.00 |  | 1.00 |  |  |  | 0.00 |  | 1.00 | 1.00 |  | 0.00 |
| Lane Grp Cap(c), veh/h 606 | 0 | 539 |  |  |  | 0 | 732 | 608 | 224 | 1047 | 0 |
| V/C Ratio(X) 0.92 | 0.00 | 0.86 |  |  |  | 0.00 | 0.66 | 0.07 | 0.86 | 0.27 | 0.00 |
| Avail Cap(c_a), veh/h 641 | 0 | 570 |  |  |  | 0 | 732 | 608 | 326 | 1047 | 0 |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) $\quad 1.00$ | 0.00 | 1.00 |  |  |  | 0.00 | 1.00 | 1.00 | 0.93 | 0.93 | 0.00 |
| Uniform Delay (d), s/veh 34.7 | 0.0 | 33.7 |  |  |  | 0.0 | 27.2 | 20.7 | 47.1 | 12.3 | 0.0 |
| Incr Delay (d2), s/veh 18.6 | 0.0 | 12.4 |  |  |  | 0.0 | 4.5 | 0.2 | 13.2 | 0.6 | 0.0 |
| Initial Q Delay(d3),s/veh 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh//h7. 2 | 0.0 | 13.2 |  |  |  | 0.0 | 11.0 | 0.7 | 5.9 | 3.7 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d), s/veh 53.4 | 0.0 | 46.1 |  |  |  | 0.0 | 31.7 | 21.0 | 60.3 | 12.9 | 0.0 |
| LnGrp LOS D | A | D |  |  |  | A | C | C | E | B | A |
| Approach Vol, veh/h | 1025 |  |  |  |  |  | 524 |  |  | 475 |  |
| Approach Delay, s/veh | 50.1 |  |  |  |  |  | 30.8 |  |  | 32.1 |  |
| Approach LOS | D |  |  |  |  |  | C |  |  | C |  |
| Timer - Assigned Phs 1 | 2 |  | 4 |  | 6 |  |  |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), $\$ 8.6$ | 48.5 |  | 42.8 |  | 67.2 |  |  |  |  |  |  |
| Change Period (Y+Rc), s* 4.7 | 5.1 |  | 5.1 |  | 5.1 |  |  |  |  |  |  |
| Max Green Setting (Gmax) 28 | 34.9 |  | 39.9 |  | 34.9 |  |  |  |  |  |  |
| Max Q Clear Time (g_c+ $\mathrm{m} / \mathrm{l}, \mathrm{T}$ | 25.2 |  | 35.5 |  | 10.6 |  |  |  |  |  |  |
| Green Ext Time (p_c), s 0.3 | 2.2 |  | 2.2 |  | 1.7 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay 40.9 |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  | D |  |  |  |  |  |  |  |  |  |

## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Intersection |
| :--- |
| Intersection Delay, s/veh14.6 |
| Intersection LOS $\quad$ B |


| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | M |  |  | $\uparrow$ | 44 | 7 |
| Traffic Vol, veh/h | 165 | 19 | 16 | 368 | 457 | 255 |
| Future Vol, veh/h | 165 | 19 | 16 | 368 | 457 | 255 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mumt Flow | 174 | 20 | 17 | 387 | 481 | 268 |
| Number of Lanes | 1 | 0 | 0 | 1 | 2 | 1 |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| Opposing Approach |  | SB | NB |
| Opposing Lanes | 0 | 3 | 1 |
| Conflicting Approach Left SB | EB |  |  |
| Conflicting Lanes Left | 3 | 1 | 0 |
| Conflicting Approach RighNB |  | EB |  |
| Conflicting Lanes Right | 1 | 0 | 1 |
| HCM Control Delay | 15.1 | 21.7 | 10.6 |
| HCM LOS | C | C | B |


| Lane | NBLn1 EBLn1 SBLn1 SBLn2 SBLn3 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $4 \%$ | $90 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $96 \%$ | $0 \%$ | $100 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, \% | $0 \%$ | $10 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 384 | 184 | 229 | 229 | 255 |
| LT Vol | 16 | 165 | 0 | 0 | 0 |
| Through Vol | 368 | 0 | 229 | 229 | 0 |
| RT Vol | 0 | 19 | 0 | 0 | 255 |
| Lane Flow Rate | 404 | 194 | 241 | 241 | 268 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.692 | 0.399 | 0.392 | 0.392 | 0.252 |
| Departure Headway (Hd) | 6.161 | 7.421 | 5.873 | 5.873 | 3.386 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 586 | 484 | 611 | 611 | 1055 |
| Service Time | 3.909 | 5.176 | 3.617 | 3.617 | 1.129 |
| HCM Lane V/C Ratio | 0.689 | 0.401 | 0.394 | 0.394 | 0.254 |
| HCM Control Delay | 21.7 | 15.1 | 12.4 | 12.4 | 7.3 |
| HCM Lane LOS | C | C | B | B | A |
| HCM 95th-tile Q | 5.4 | 1.9 | 1.9 | 1.9 | 1 |

Intersection
Intersection Delay, s/veh 17
Intersection LOS $\quad$ C


| Lane | NBLn1WBLn1 WBLn2 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $100 \%$ | $0 \%$ | $97 \%$ |
| Vol Thru, \% | $74 \%$ | $0 \%$ | $0 \%$ | $3 \%$ |
| Vol Right, \% | $26 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 57 | 16 | 343 | 473 |
| LT Vol | 0 | 16 | 0 | 459 |
| Through Vol | 42 | 0 | 0 | 14 |
| RT Vol | 15 | 0 | 343 | 0 |
| Lane Flow Rate | 59 | 16 | 354 | 488 |
| Geometry Grp | 2 | 7 | 7 | 2 |
| Degree of Util (X) | 0.091 | 0.03 | 0.526 | 0.714 |
| Departure Headway (Hd) | 5.575 | 6.566 | 5.351 | 5.274 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 662 | 546 | 675 | 688 |
| Service Time | 3.613 | 4.293 | 3.078 | 3.298 |
| HCM Lane V/C Ratio | 0.002 | 0.029 | 0.524 | 0.709 |
| HCM Control Delay | 9.2 | 9.5 | 13.9 | 20.4 |
| HCM Lane LOS | A | A | B | C |
| HCM 95th-tile Q | 0.3 | 0.1 | 3.1 | 6 |

6: Clearwater Way \& Dairy Mart Rd


| Major/Minor M | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 50 | 0 | 105 | 49 |
| Stage 1 | - | - | - | - | 49 | - |
| Stage 2 | - | - | - | - | 56 | - |
| Critical Hdwy | - | - | 4.13 | - | 6.43 | 6.23 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.43 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.43 | - |
| Follow-up Hdwy | - | - | 2.227 | - | 3.527 | 3.327 |
| Pot Cap-1 Maneuver | - | - | 1550 | - | 890 | 1017 |
| Stage 1 | - | - | - | - | 971 | - |
| Stage 2 | - | - | - | - | 964 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1550 | - | 887 | 1017 |
| Mov Cap-2 Maneuver | - | - | - | - | 887 | - |
| Stage 1 | - | - | - | - | 971 | - |
| Stage 2 | - | - | - | - | 961 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.7 |  | 8.7 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | WBL WBT |  |
| Capacity (veh/h) |  | 81 | - | - | 1550 | - |
| HCM Lane V/C Ratio |  | 15 | - | - | 0.003 | - |
| HCM Control Delay (s) |  | 8.7 | - | - | 7.3 | - |
| HCM Lane LOS |  | A | - | - | A | - |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\hat{\imath}$ |  |  | - | r |  |
| Traffic Vol, veh/h | 27 | 1 | 2 | 32 | 2 | 15 |
| Future Vol, veh/h | 27 | 1 | 2 | 32 | 2 | 15 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 82 | 82 | 82 | 82 | 82 | 82 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 33 | 1 | 2 | 39 | 2 | 18 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.9 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | -1 | $\hat{l}$ |  | M |  |
| Traffic Vol, veh/h | 8 | 6 | 8 | 21 | 17 | 5 |
| Future Vol, veh/h | 8 | 6 | 8 | 21 | 17 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 76 | 76 | 76 | 76 | 76 | 76 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 11 | 8 | 11 | 28 | 22 | 7 |


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 39 | 0 | - | 0 | 55 | 25 |
| Stage 1 | - | - | - - | - | 25 | - |
| Stage 2 | - | - | - - | - | 30 | - |
| Critical Hdwy | 4.13 | - | - - | - | 6.43 | 6.23 |
| Critical Hdwy Stg 1 | - | - | - - | - | 5.43 | - |
| Critical Hdwy Stg 2 | - | - | - - | - | 5.43 | - |
| Follow-up Hdwy | 2.227 | - | - - | - | 3.527 | 3.327 |
| Pot Cap-1 Maneuver | 1565 | - | - - | - | 950 | 1048 |
| Stage 1 | - | - | - - | - | 995 | - |
| Stage 2 | - | - | - - | - | 990 | - |
| Platoon blocked, \% |  | - | - - | - |  |  |
| Mov Cap-1 Maneuver | 1565 | - | - - | - | 943 | 1048 |
| Mov Cap-2 Maneuver | - | - | - - | - | 943 | - |
| Stage 1 | - | - | - - | - | 988 | - |
| Stage 2 | - | - | - - | - | 990 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 4.2 |  | 0 |  | 8.8 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1565 |  | - | - | 965 |
| HCM Lane V/C Ratio |  | 0.007 | - | - | - | 0.03 |
| HCM Control Delay (s) |  | 7.3 | 0 | - | - | 8.8 |
| HCM Lane LOS |  | A | A | - | - | A |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | 0.1 |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 个 $\uparrow$ |  | \% | 个 |  | * | ¢ |  | \% | $\stackrel{1}{6}$ |  |
| Traffic Volume (veh/h) | 7 | 35 | 2 | 91 | 49 | 382 | 1 | 52 | 84 | 465 | 61 | 13 |
| Future Volume (veh/h) | 7 | 35 | 2 | 91 | 49 | 382 | 1 | 52 | 84 | 465 | 61 | 13 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 0.97 | 1.00 |  | 0.98 | 1.00 |  | 0.98 | 1.00 |  | 0.98 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 |
| Adj Flow Rate, veh/h | 7 | 37 | 2 | 96 | 52 | 402 | 1 | 55 | 88 | 489 | 64 | 14 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, \% | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 16 | 636 | 34 | 122 | 436 | 380 | 2 | 155 | 248 | 534 | 800 | 175 |
| Arrive On Green | 0.01 | 0.19 | 0.19 | 0.07 | 0.25 | 0.25 | 0.00 | 0.24 | 0.24 | 0.30 | 0.54 | 0.54 |
| Sat Flow, veh/h | 1767 | 3397 | 182 | 1767 | 1763 | 1536 | 1767 | 635 | 1016 | 1767 | 1470 | 322 |
| Grp Volume(v), veh/h | 7 | 19 | 20 | 96 | 52 | 402 | 1 | 0 | 143 | 489 | 0 | 78 |
| Grp Sat Flow(s),veh/h/ln | 1767 | 1763 | 1817 | 1767 | 1763 | 1536 | 1767 | 0 | 1651 | 1767 | 0 | 1791 |
| Q Serve(g_s), s | 0.4 | 0.8 | 0.8 | 4.9 | 2.1 | 22.5 | 0.1 | 0.0 | 6.5 | 24.3 | 0.0 | 1.9 |
| Cycle Q Clear (g_c), s | 0.4 | 0.8 | 0.8 | 4.9 | 2.1 | 22.5 | 0.1 | 0.0 | 6.5 | 24.3 | 0.0 | 1.9 |
| Prop In Lane | 1.00 |  | 0.10 | 1.00 |  | 1.00 | 1.00 |  | 0.62 | 1.00 |  | 0.18 |
| Lane Grp Cap (c), veh/h | 16 | 330 | 340 | 122 | 436 | 380 | 2 | 0 | 402 | 534 | 0 | 975 |
| V/C Ratio(X) | 0.44 | 0.06 | 0.06 | 0.78 | 0.12 | 1.06 | 0.41 | 0.00 | 0.36 | 0.92 | 0.00 | 0.08 |
| Avail Cap(c_a), veh/h | 97 | 349 | 360 | 185 | 436 | 380 | 97 | 0 | 402 | 690 | 0 | 975 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 44.8 | 30.4 | 30.4 | 41.7 | 26.5 | 34.2 | 45.4 | 0.0 | 28.5 | 30.6 | 0.0 | 9.9 |
| Incr Delay (d2), s/veh | 18.4 | 0.1 | 0.1 | 11.8 | 0.1 | 62.3 | 85.2 | 0.0 | 2.4 | 14.5 | 0.0 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.2 | 0.4 | 0.4 | 2.5 | 0.9 | 14.6 | 0.1 | 0.0 | 2.8 | 12.1 | 0.0 | 0.7 |

Unsig. Movement Delay, s/veh

| LnGrp Delay(d),s/veh | 63.2 | 30.4 | 30.5 | 53.5 | 26.7 | 96.5 | 130.6 | 0.0 | 30.9 | 45.1 | 0.0 | 10.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LnGrp LOS | E | C | C | D | C | F | F | A | C | D | A | B |
| Approach Vol, veh/h |  | 46 |  |  | 550 |  |  | 144 |  | 567 |  |  |
| Approach Delay, s/veh |  | 35.4 |  |  | 82.4 |  |  | 31.6 |  | 40.3 |  |  |
| Approach LOS |  | D |  |  | F |  |  | C |  | D |  |  |


| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), s | 32.0 | 26.7 | 10.8 | 21.5 | 4.6 | 54.0 | 5.3 | 27.0 |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax), s | 35.5 | 19.0 | 9.5 | 18.0 | 5.0 | 49.5 | 5.0 | 22.5 |
| Max Q Clear Time (g_c+11), s | 26.3 | 8.5 | 6.9 | 2.8 | 2.1 | 3.9 | 2.4 | 24.5 |
| Green Ext Time (p_c), s | 1.2 | 0.5 | 0.0 | 0.1 | 0.0 | 0.4 | 0.0 | 0.0 |

Intersection Summary

| HCM 6th Ctrl Delay | 56.9 |
| :--- | ---: |
| HCM 6th LOS | $E$ |

- Opening Year Conditions



## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ＋ | 7 | \％ | 4 | 「 | \％ | 4 | 「 | ${ }^{7}$ | 4 | $\stackrel{7}{ }$ |
| Traffic Volume（veh／h） 30 | 272 | 61 | 62 | 114 | 162 | 132 | 168 | 562 | 209 | 87 | 53 |
| Future Volume（veh／h） 30 | 272 | 61 | 62 | 114 | 162 | 132 | 168 | 562 | 209 | 87 | 53 |
| Initial Q（Qb），veh 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） 1.00 |  | 0.98 | 1.00 |  | 0.98 | 0.99 |  | 0.99 | 1.00 |  | 1.00 |
| Parking Bus，Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 |
| Adj Flow Rate，veh／h 35 | 316 | 71 | 72 | 133 | 188 | 153 | 195 | 653 | 243 | 101 | 0 |
| Peak Hour Factor 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Percent Heavy Veh，\％ 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap，veh／h 63 | 409 | 341 | 98 | 446 | 369 | 677 | 619 | 605 | 481 | 685 |  |
| Arrive On Green 0.04 | 0.22 | 0.22 | 0.06 | 0.24 | 0.24 | 0.08 | 0.33 | 0.33 | 0.12 | 0.37 | 0.00 |
| Sat Flow，veh／h 1767 | 1856 | 1544 | 1767 | 1856 | 1537 | 1767 | 1856 | 1554 | 1767 | 1856 | 1572 |
| Grp Volume（v），veh／h 35 | 316 | 71 | 72 | 133 | 188 | 153 | 195 | 653 | 243 | 101 | 0 |
| Grp Sat Flow（s），veh／h／ln1767 | 1856 | 1544 | 1767 | 1856 | 1537 | 1767 | 1856 | 1554 | 1767 | 1856 | 1572 |
| Q Serve（g＿s），s 1.3 | 10.6 | 2.5 | 2.6 | 3.9 | 7.0 | 3.7 | 5.2 | 22.0 | 5.8 | 2.4 | 0.0 |
| Cycle Q Clear（g＿c），s 1.3 | 10.6 | 2.5 | 2.6 | 3.9 | 7.0 | 3.7 | 5.2 | 22.0 | 5.8 | 2.4 | 0.0 |
| Prop In Lane 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h 63 | 409 | 341 | 98 | 446 | 369 | 677 | 619 | 605 | 481 | 685 |  |
| V／C Ratio（X） 0.55 | 0.77 | 0.21 | 0.73 | 0.30 | 0.51 | 0.23 | 0.32 | 1.08 | 0.50 | 0.15 |  |
| Avail Cap（c＿a），veh／h 241 | 619 | 515 | 241 | 619 | 512 | 773 | 619 | 605 | 514 | 685 |  |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay（d），s／veh 31.3 | 24.2 | 21.0 | 30.7 | 20.5 | 21.7 | 12.3 | 16.4 | 20.2 | 11.9 | 13.9 | 0.0 |
| Incr Delay（d2），s／veh 7.3 | 3.4 | 0.3 | 10.1 | 0.4 | 1.1 | 0.2 | 1.3 | 59.7 | 0.8 | 0.5 | 0.0 |
| Initial Q Delay（d3），s／veh 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／lm0．7 | 4.7 | 0.9 | 1.4 | 1.6 | 2.5 | 1.3 | 2.3 | 18.3 | 2.1 | 1.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh 38.6 | 27.5 | 21.3 | 40.8 | 20.9 | 22.8 | 12.5 | 17.7 | 79.9 | 12.7 | 14.4 | 0.0 |
| LnGrp LOS D | C | C | D | C | C | B | B | F | B | B |  |
| Approach Vol，veh／h | 422 |  |  | 393 |  |  | 1001 |  |  | 344 | A |
| Approach Delay，s／veh | 27.4 |  |  | 25.4 |  |  | 57.5 |  |  | 13.2 |  |
| Approach LOS | C |  |  | C |  |  | E |  |  | B |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），$\$ 2.3$ | 26.5 | 8.2 | 19.1 | 9.9 | 28.9 | 6.9 | 20.4 |  |
| Change Period（Y＋Rc），s 4．5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |  |
| Max Green Setting（Gmax9．8 | 22.0 | 9.0 | 22.0 | 9.0 | 22.0 | 9.0 | 22.0 |  |
| Max Q Clear Time（g＿c＋I1才，© | 24.0 | 4.6 | 12.6 | 5.7 | 4.4 | 3.3 | 9.0 |  |
| Green Ext Time（p＿c），s | 0.1 | 0.0 | 0.0 | 1.4 | 0.1 | 0.4 | 0.0 | 1.1 |

Intersection Summary

| HCM 6th Ctrl Delay | 38.7 |
| :--- | ---: |
| HCM 6th LOS | $D$ |

## Notes

Unsignalized Delay for［SBR］is excluded from calculations of the approach delay and intersection delay．



## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.


Intersection Delay, s/veh18.6
Intersection LOS

| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Configurations | N |  |  | $\uparrow$ | 4 | $\boldsymbol{\top}$ |
| Traffic Vol, veh/h | 266 | 20 | 6 | 340 | 334 | 114 |
| Future Vol, veh/h | 266 | 20 | 6 | 340 | 334 | 114 |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 302 | 23 | 7 | 386 | 380 | 130 |
| Number of Lanes | 1 | 0 | 0 | 1 | 2 | 1 |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| Opposing Approach |  | SB | NB |
| Opposing Lanes | 0 | 3 | 1 |
| Conflicting Approach Left SB | EB |  |  |
| Conflicting Lanes Left | 3 | 1 | 0 |
| Conflicting Approach RighNB |  | EB |  |
| Conflicting Lanes Right | 1 | 0 | 1 |
| HCM Control Delay | 23 | 24.4 | 11.4 |
| HCM LOS | C | C | B |


| Lane | NBLn1 EBLn1 SBLn1 SBLn2 SBLn3 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $2 \%$ | $93 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $98 \%$ | $0 \%$ | $100 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, \% | $0 \%$ | $7 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 346 | 286 | 167 | 167 | 114 |
| LT Vol | 6 | 266 | 0 | 0 | 0 |
| Through Vol | 340 | 0 | 167 | 167 | 0 |
| RT Vol | 0 | 20 | 0 | 0 | 114 |
| Lane Flow Rate | 393 | 325 | 190 | 190 | 130 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.717 | 0.657 | 0.342 | 0.342 | 0.144 |
| Departure Headway (Hd) | 6.567 | 7.281 | 6.497 | 6.497 | 3.996 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 547 | 494 | 550 | 550 | 883 |
| Service Time | 4.351 | 5.055 | 4.284 | 4.284 | 1.781 |
| HCM Lane V/C Ratio | 0.718 | 0.658 | 0.345 | 0.345 | 0.147 |
| HCM Control Delay | 24.4 | 23 | 12.7 | 12.7 | 7.5 |
| HCM Lane LOS | C | C | B | B | A |
| HCM 95th-tile Q | 5.8 | 4.7 | 1.5 | 1.5 | 0.5 |

Intersection

Intersection Delay, s/veh12.6
Intersection LOS B


| Lane | NBLn1WBLn1 WBLn2 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $100 \%$ | $0 \%$ | $49 \%$ |
| Vol Thru, \% | $84 \%$ | $0 \%$ | $0 \%$ | $51 \%$ |
| Vol Right, \% | $16 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 37 | 7 | 319 | 346 |
| LT Vol | 0 | 7 | 0 | 169 |
| Through Vol | 31 | 0 | 0 | 177 |
| RT Vol | 6 | 0 | 319 | 0 |
| Lane Flow Rate | 41 | 8 | 351 | 380 |
| Geometry Grp | 2 | 7 | 7 | 2 |
| Degree of Util (X) | 0.06 | 0.013 | 0.478 | 0.526 |
| Departure Headway (Hd) | 5.351 | 6.119 | 4.908 | 4.985 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 663 | 582 | 729 | 719 |
| Service Time | 3.351 | 3.885 | 2.674 | 3.057 |
| HCM Lane V/C Ratio | 0.061 | 0.014 | 0.481 | 0.529 |
| HCM Control Delay | 8.7 | 9 | 12.1 | 13.5 |
| HCM Lane LOS | A | A | B | B |
| HCM 95th-tile Q | 0.2 | 0 | 2.6 | 3.1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.4 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  | 1 | 4 | ri |  |
| Traffic Vol, veh/h | 34 | 6 | 26 | 172 | 7 | 8 |
| Future Vol, veh/h | 34 | 6 | 26 | 172 | 7 | 8 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 235 | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 79 | 79 | 79 | 79 | 79 | 79 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 43 | 8 | 33 | 218 | 9 | 10 |


| Major/Minor | Major1 | Major2 |  | Minor1 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 0 | 0 | 51 | 0 | 331 | 47 |
| $\quad$ Stage 1 | - | - | - | - | 47 | - |
| $\quad$ Stage 2 | - | - | - | - | 284 | - |
| Critical Hdwy | - | - | 4.13 | - | 6.43 | 6.23 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.43 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.43 | - |
| Follow-up Hdwy | - | - | 2.227 | - | 3.527 | 3.327 |
| Pot Cap-1 Maneuver | - | - | 1549 | - | 662 | 1019 |
| $\quad$ Stage 1 | - | - | - | - | 973 | - |
| $\quad$ Stage 2 | - | - | - | - | 762 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1549 | - | 648 | 1019 |
| Mov Cap-2 Maneuver | - | - | - | - | 648 | - |
| Stage 1 | - | - | - | - | 973 | - |
| Stage 2 | - | - | - | - | 746 | - |
|  |  |  |  |  |  |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | :--- |
| HCM Control Delay, $s$ | 0 | 1 | 9.6 |

HCM LOS A

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 804 | - | -1549 | - |  |
| HCM Lane V/C Ratio | 0.024 | - | -0.021 | - |  |
| HCM Control Delay (s) | 9.6 | - | - | 7.4 | - |
| HCM Lane LOS | A | - | - | A | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | - | 0.1 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | $\uparrow$ | r |  |
| Traffic Vol, veh/h | 27 | 0 | 18 | 156 | 2 | 6 |
| Future Vol, veh/h | 27 | 0 | 18 | 156 | 2 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 61 | 61 | 61 | 61 | 61 | 61 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 44 | 0 | 30 | 256 | 3 | 10 |


| Major/Minor | Major1 | Major2 |  |  | Minor1 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Conflicting Flow All | 0 | 0 | 44 | 0 | 360 | 44 |  |
| Stage 1 | - | - | - | - | 44 | - |  |
| Stage 2 | - | - | - | - | 316 | - |  |
| Critical Hdwy | - | - | 4.13 | - | 6.43 | 6.23 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.43 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.43 | - |  |
| Follow-up Hdwy | - | - | 2.227 | - | 3.527 | 3.327 |  |
| Pot Cap-1 Maneuver | - | - | 1558 | - | 637 | 1023 |  |
| Stage 1 | - | - | - | - | 976 | - |  |
| Stage 2 | - | - | - | - | 737 | - |  |
| Platoon blocked, \% | - | - |  | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | 1558 | - | 623 | 1023 |  |
| Mov Cap-2 Maneuver | - | - | - | - | 623 | - |  |
| Stage 1 | - | - | - | - | 976 | - |  |
| Stage 2 | - | - | - | - | 721 | - |  |


| Approach | EB | WB | NB |
| :--- | ---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.8 | 9.1 |

HCMLOS A

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacity (veh/h) | 882 | - | - | 1558 | - |  |
| HCM Lane V/C Ratio | 0.015 | - | - | 0.019 | - |  |
| HCM Control Delay (s) | 9.1 | - | - | 7.4 | 0 |  |
| HCM Lane LOS | A | - | - | A | A |  |
| HCM 95th \%tile Q(veh) | 0 | - | - | 0.1 | - |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.5 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | -1 | 1 |  | M |  |
| Traffic Vol, veh/h | 13 | 18 | 142 | 5 | 6 | 43 |
| Future Vol, veh/h | 13 | 18 | 142 | 5 | 6 | 43 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 88 | 88 | 88 | 88 | 88 | 88 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 15 | 20 | 161 | 6 | 7 | 49 |



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{*}$ | 个t |  | * | 㻢 |  | ${ }^{7}$ | $\hat{p}$ |  | \% | $\uparrow$ |  |
| Traffic Volume (veh/h) | 33 | 50 | 2 | 84 | 24 | 555 | 0 | 74 | 102 | 472 | 60 | 21 |
| Future Volume (veh/h) | 33 | 50 | 2 | 84 | 24 | 555 | 0 | 74 | 102 | 472 | 60 | 21 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 0.99 | 1.00 |  | 0.99 | 1.00 |  | 0.97 | 1.00 |  | 0.98 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 |
| Adj Flow Rate, veh/h | 41 | 62 | 2 | 104 | 30 | 685 | 0 | 91 | 126 | 583 | 74 | 26 |
| Peak Hour Factor | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 |
| Percent Heavy Veh, \% | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 59 | 923 | 30 | 132 | 540 | 477 | 2 | 212 | 294 | 321 | 692 | 243 |
| Arrive On Green | 0.03 | 0.26 | 0.26 | 0.07 | 0.31 | 0.31 | 0.00 | 0.31 | 0.31 | 0.18 | 0.53 | 0.53 |
| Sat Flow, veh/h | 1767 | 3485 | 112 | 1767 | 1763 | 1557 | 1767 | 693 | 960 | 1767 | 1304 | 458 |
| Grp Volume(v), veh/h | 41 | 31 | 33 | 104 | 30 | 685 | 0 | 0 | 217 | 583 | 0 | 100 |
| Grp Sat Flow(s),veh/h/ln | 1767 | 1763 | 1834 | 1767 | 1763 | 1557 | 1767 | 0 | 1653 | 1767 | 0 | 1762 |
| Q Serve(g_s), s | 2.4 | 1.4 | 1.4 | 6.0 | 1.3 | 32.0 | 0.0 | 0.0 | 11.0 | 19.0 | 0.0 | 2.9 |
| Cycle Q Clear(g_c), s | 2.4 | 1.4 | 1.4 | 6.0 | 1.3 | 32.0 | 0.0 | 0.0 | 11.0 | 19.0 | 0.0 | 2.9 |
| Prop In Lane | 1.00 |  | 0.06 | 1.00 |  | 1.00 | 1.00 |  | 0.58 | 1.00 |  | 0.26 |
| Lane Grp Cap(c), veh/h | 59 | 467 | 486 | 132 | 540 | 477 | 2 | 0 | 506 | 321 | 0 | 936 |
| V/C Ratio(X) | 0.70 | 0.07 | 0.07 | 0.79 | 0.06 | 1.44 | 0.00 | 0.00 | 0.43 | 1.81 | 0.00 | 0.11 |
| Avail Cap(c_a), veh/h | 321 | 540 | 562 | 321 | 540 | 477 | 321 | 0 | 506 | 321 | 0 | 936 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 50.0 | 28.7 | 28.7 | 47.5 | 25.6 | 36.2 | 0.0 | 0.0 | 28.9 | 42.7 | 0.0 | 12.2 |
| Incr Delay (d2), s/veh | 13.8 | 0.1 | 0.1 | 9.9 | 0.0 | 208.1 | 0.0 | 0.0 | 2.6 | 378.4 | 0.0 | 0.2 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.3 | 0.6 | 0.6 | 3.0 | 0.5 | 39.3 | 0.0 | 0.0 | 4.7 | 42.0 | 0.0 | 1.2 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 63.8 | 28.8 | 28.8 | 57.4 | 25.6 | 244.3 | 0.0 | 0.0 | 31.6 | 421.2 | 0.0 | 12.4 |
| LnGrp LOS | E | C | C | E | C | F | A | A | C | F | A | B |
| Approach Vol, veh/h |  | 105 |  |  | 819 |  |  | 217 |  |  | 683 |  |
| Approach Delay, s/veh |  | 42.5 |  |  | 212.6 |  |  | 31.6 |  |  | 361.3 |  |
| Approach LOS |  | D |  |  | F |  |  | C |  |  | F |  |


| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), s | 23.5 | 36.5 | 12.3 | 32.2 | 0.0 | 60.0 | 8.0 | 36.5 |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax), s | 19.0 | 32.0 | 19.0 | 32.0 | 19.0 | 32.0 | 19.0 | 32.0 |
| Max Q Clear Time (g_c+I1), s | 21.0 | 13.0 | 8.0 | 3.4 | 0.0 | 4.9 | 4.4 | 34.0 |
| Green Ext Time (p_c), s | 0.0 | 1.2 | 0.2 | 0.3 | 0.0 | 0.5 | 0.1 | 0.0 |

Intersection Summary
HCM 6th Ctrl Delay 236.9

HCM 6th LOS
F

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Y |  |  | A | l |  |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 0 | 0 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 0 | 0 |


| Major/Minor | Minor2 | Major1 |  | Major2 |  |  |
| :--- | ---: | ---: | ---: | :--- | :--- | :--- |
| Conflicting Flow All | 1 | 1 | 1 | 0 | - | 0 |
| $\quad$ Stage 1 | 1 | - | - | - | - | - |
| $\quad$ Stage 2 | 0 | - | - | - | - | - |
| Critical Hdwy | 6.43 | 6.23 | 4.13 | - | - | - |
| Critical Hdwy Stg 1 | 5.43 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.43 | - | - | - | - | - |
| Follow-up Hdwy | 3.527 | 3.327 | 2.227 | - | - | - |
| Pot Cap-1 Maneuver | 1019 | 1081 | 1615 | - | - | - |
| $\quad$ Stage 1 | 1020 | - | - | - | - | - |
| $\quad$ Stage 2 | - | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 1019 | 1081 | 1615 | - | - | - |
| Mov Cap-2 Maneuver | 1019 | - | - | - | - | - |
| Stage 1 | 1020 | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
|  |  |  |  |  |  |  |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 0 |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1615 | - | - | - | - |
| HCM Lane V/C Ratio | - | - | - | - | - |
| HCM Control Delay (s) | 0 | - | 0 | - | - |
| HCM Lane LOS | A | - | A | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | - | - | - |



## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Lane Configurations | \% | 4 |  | \% | 4 | 7 | \% | 4 | 7 | \% | 4 | 7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Future Volume (veh/h) | 27 | 180 | 112 | 161 | 103 | 156 | 153 | 237 | 810 | 219 | 213 | 58 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 0.94 | 1.00 |  | 0.97 | 0.99 |  | 0.96 | 1.00 |  | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Flow Rate, veh/h | 28 | 188 | 117 | 168 | 107 | 162 | 159 | 247 | 844 | 228 | 222 | 0 |
| Percent Heavy Veh, \% | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Arrive On Green | 0.03 | 0.17 | 0.17 | 0.12 | 0.26 | 0.26 | 0.08 | 0.37 | 0.37 | 0.11 | 0.40 | 0.00 |
| Grp Volume(v), veh/h | 28 | 188 | 117 | 168 | 107 | 162 | 159 | 247 | 844 | 228 | 222 | 0 |
| Q Serve(g_s), s | 1.2 | 7.2 | 5.5 | 7.1 | 3.5 | 6.8 | 4.2 | 7.4 | 28.4 | 6.0 | 6.3 | 0.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| V/C Ratio(X) | 0.54 | 0.60 | 0.47 | 0.78 | 0.22 | 0.41 | 0.27 | 0.36 | 1.13 | 0.54 | 0.30 |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 36.8 | 29.6 | 28.9 | 32.8 | 22.3 | 23.6 | 12.9 | 17.6 | 19.7 | 12.7 | 15.9 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

## Unsig. Movement Delay, s/veh

| $\operatorname{Ln} G r p$ |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| LOS | D | C | C | D | C | C | B | B | F | B | B |
|  |  |  |  |  |  |  |  |  |  |  |  |


| Approach Delay, s/veh | 32.2 |  |  | 29.5 |  |  | 69.2 | 15.3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |  |
| Max Q Clear Time (g_c+19, ©s | 30.4 | 9.1 | 9.2 | 6.2 | 8.3 | 3.2 | 8.8 |  |
|  |  |  |  |  |  |  |  |  |
| $y$ |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr Delay |  | 47.4 |  |  |  |  |  |  |
| HCM 6th LOS |  | D |  |  |  |  |  |  |

## Notes

Unsignalized Delay for [SBR] is excluded from calculations of the approach delay and intersection delay.

| 4 |  | $\square$ |  | $\Perp$ |  | 4 | 4 | \% | - | 1 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 4 | F |  |  |  |  | 4 | F | ${ }^{7}$ | 4 |  |
| Traffic Volume (veh/h) 581 | 1 | 491 | 0 | 0 | 0 | 0 | 623 | 57 | 193 | 293 | 0 |
| Future Volume (veh/h) 581 | 1 | 491 | 0 | 0 | 0 | 0 | 623 | 57 | 193 | 293 | 0 |
| Initial Q $(\mathrm{Qb})$, veh 0 | 0 | 0 |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) 1.00 |  | 1.00 |  |  |  | 1.00 |  | 0.98 | 1.00 |  | 1.00 |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  |  |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln 1856 | 1856 | 1856 |  |  |  | 0 | 1856 | 1856 | 1856 | 1856 | 0 |
| Adj Flow Rate, veh/h 593 | 1 | 501 |  |  |  | 0 | 636 | 58 | 197 | 299 | 0 |
| Peak Hour Factor 0.98 | 0.98 | 0.98 |  |  |  | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Percent Heavy Veh, \% 3 | 3 | 3 |  |  |  | 0 | 3 | 3 | 3 | 3 | 0 |
| Cap, veh/h 627 | 1 | 558 |  |  |  | 0 | 704 | 584 | 229 | 1024 | 0 |
| Arrive On Green 0.36 | 0.36 | 0.36 |  |  |  | 0.00 | 0.38 | 0.38 | 0.13 | 0.55 | 0.00 |
| Sat Flow, veh/h 1764 | 3 | 1571 |  |  |  | 0 | 1856 | 1540 | 1767 | 1856 | 0 |
| Grp Volume(v), veh/h 594 | 0 | 501 |  |  |  | 0 | 636 | 58 | 197 | 299 | 0 |
| Grp Sat Flow(s),veh/h/ln1767 | 0 | 1571 |  |  |  | 0 | 1856 | 1540 | 1767 | 1856 | 0 |
| Q Serve(g_s), s 35.9 | 0.0 | 33.2 |  |  |  | 0.0 | 35.6 | 2.7 | 12.0 | 9.5 | 0.0 |
| Cycle Q Clear(g_c), s 35.9 | 0.0 | 33.2 |  |  |  | 0.0 | 35.6 | 2.7 | 12.0 | 9.5 | 0.0 |
| Prop In Lane 1.00 |  | 1.00 |  |  |  | 0.00 |  | 1.00 | 1.00 |  | 0.00 |
| Lane Grp Cap(c), veh/h 628 | 0 | 558 |  |  |  | 0 | 704 | 584 | 229 | 1024 | 0 |
| V/C Ratio(X) 0.95 | 0.00 | 0.90 |  |  |  | 0.00 | 0.90 | 0.10 | 0.86 | 0.29 | 0.00 |
| Avail Cap(c_a), veh/h 641 | 0 | 570 |  |  |  | 0 | 704 | 584 | 326 | 1024 | 0 |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) $\quad 1.00$ | 0.00 | 1.00 |  |  |  | 0.00 | 1.00 | 1.00 | 0.94 | 0.94 | 0.00 |
| Uniform Delay (d), s/veh 34.4 | 0.0 | 33.6 |  |  |  | 0.0 | 32.2 | 22.0 | 46.9 | 13.2 | 0.0 |
| Incr Delay (d2), s/veh 22.8 | 0.0 | 16.7 |  |  |  | 0.0 | 17.1 | 0.3 | 14.1 | 0.7 | 0.0 |
| Initial Q Delay(d3),s/veh 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/1/h9.0 | 0.0 | 15.0 |  |  |  | 0.0 | 18.9 | 1.0 | 6.2 | 4.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d), s/veh 57.3 | 0.0 | 50.3 |  |  |  | 0.0 | 49.3 | 22.3 | 61.0 | 13.8 | 0.0 |
| LnGrp LOS E | A | D |  |  |  | A | D | C | E | B | A |
| Approach Vol, veh/h | 1095 |  |  |  |  |  | 694 |  |  | 496 |  |
| Approach Delay, s/veh | 54.1 |  |  |  |  |  | 47.1 |  |  | 32.6 |  |
| Approach LOS | D |  |  |  |  |  | D |  |  | C |  |
| Timer - Assigned Phs 1 | 2 |  | 4 |  | 6 |  |  |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), $\$ 9.0$ | 46.9 |  | 44.2 |  | 65.8 |  |  |  |  |  |  |
| Change Period (Y+Rc), s* 4.7 | 5.1 |  | 5.1 |  | 5.1 |  |  |  |  |  |  |
| Max Green Setting (Gmak)28 | 34.9 |  | 39.9 |  | 34.9 |  |  |  |  |  |  |
| Max Q Clear Time (g_c+MIIL, ©s | 37.6 |  | 37.9 |  | 11.5 |  |  |  |  |  |  |
| Green Ext Time (p_c), s 0.3 | 0.0 |  | 1.2 |  | 1.8 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay 47.3 |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS D |  |  |  |  |  |  |  |  |  |  |  |

## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.
Intersection
Intersection Delay, s/veh32.7
Intersection LOS $\quad$ D

| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Configurations | M |  |  | $\uparrow$ | $\mathbf{4}$ | $\widetilde{7}$ |
| Traffic Vol, veh/h | 168 | 19 | 16 | 532 | 502 | 260 |
| Future Vol, veh/h | 168 | 19 | 16 | 532 | 502 | 260 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 177 | 20 | 17 | 560 | 528 | 274 |
| Number of Lanes | 1 | 0 | 0 | 1 | 2 | 1 |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| Opposing Approach |  | SB | NB |
| Opposing Lanes | 0 | 3 | 1 |
| Conflicting Approach Left SB | EB |  |  |
| Conflicting Lanes Left | 3 | 1 | 0 |
| Conflicting Approach RighNB |  | EB |  |
| Conflicting Lanes Right | 1 | 0 | 1 |
| HCM Control Delay | 16.8 | 67 | 12 |
| HCM LOS | C | F | B |


| Lane | NBLn1 EBLn1 SBLn1 | SBLn2 SBLn3 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $3 \%$ | $90 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $97 \%$ | $0 \%$ | $100 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, \% | $0 \%$ | $10 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 548 | 187 | 251 | 251 | 260 |
| LT Vol | 16 | 168 | 0 | 0 | 0 |
| Through Vol | 532 | 0 | 251 | 251 | 0 |
| RT Vol | 0 | 19 | 0 | 0 | 260 |
| Lane Flow Rate | 577 | 197 | 264 | 264 | 274 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 1.016 | 0.436 | 0.456 | 0.456 | 0.282 |
| Departure Headway (Hd) | 6.34 | 7.973 | 6.211 | 6.211 | 3.714 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 571 | 449 | 576 | 576 | 955 |
| Service Time | 4.112 | 5.761 | 3.986 | 3.986 | 1.488 |
| HCM Lane V/C Ratio | 1.011 | 0.439 | 0.458 | 0.458 | 0.287 |
| HCM Control Delay | 67 | 16.8 | 14.1 | 14.1 | 8 |
| HCM Lane LOS | F | C | B | B | A |
| HCM 95th-tile Q | 15.2 | 2.2 | 2.4 | 2.4 | 1.2 |


| Intersection |
| :--- |
| Intersection Delay, s/veh 23 |
| Intersection LOS C |


| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Configurations | 16 | $\mathbf{r}$ | $\hat{f}$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 16 | 350 | 200 | 17 | 468 | 50 |
| Future Vol, veh/h | 16 | 350 | 200 | 17 | 468 | 50 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 16 | 361 | 206 | 18 | 482 | 52 |
| Number of Lanes | 1 | 1 | 1 | 0 | 0 | 1 |
| Approach | WB |  | NB |  | SB |  |
| Opposing Approach |  |  | SB | NB |  |  |
| Opposing Lanes | 0 | 1 | 1 |  |  |  |
| Conflicting Approach Left NB |  |  | WB |  |  |  |
| Conflicting Lanes Left | 1 | 0 | 2 |  |  |  |
| Conflicting Approach RighISB | WB |  |  |  |  |  |
| Conflicting Lanes Right | 1 | 2 | 0 |  |  |  |
| HCM Control Delay | 16.8 | 12.5 | 31.8 |  |  |  |
| HCM LOS | C | B | D |  |  |  |


| Lane | NBLn1 WBLn1 WBLn2 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $100 \%$ | $0 \%$ | $90 \%$ |
| Vol Thru, \% | $92 \%$ | $0 \%$ | $0 \%$ | $10 \%$ |
| Vol Right, \% | $8 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 217 | 16 | 350 | 518 |
| LT Vol | 0 | 16 | 0 | 468 |
| Through Vol | 200 | 0 | 0 | 50 |
| RT Vol | 17 | 0 | 350 | 0 |
| Lane Flow Rate | 224 | 16 | 361 | 534 |
| Geometry Grp | 2 | 7 | 7 | 2 |
| Degree of Util (X) | 0.37 | 0.033 | 0.595 | 0.842 |
| Departure Headway (Hd) | 5.949 | 7.159 | 5.937 | 5.674 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 602 | 498 | 606 | 635 |
| Service Time | 4.022 | 4.927 | 3.704 | 3.73 |
| HCM Lane V/C Ratio | 0.372 | 0.032 | 0.596 | 0.841 |
| HCM Control Delay | 12.5 | 10.2 | 17.1 | 31.8 |
| HCM Lane LOS | B | B | C | D |
| HCM 95th-tile Q | 1.7 | 0.1 | 3.9 | 9.2 |



| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 230 | 0 | 330 | 229 |
| Stage 1 | - | - | - | - | 229 | - |
| Stage 2 | - | - | - | - | 101 | - |
| Critical Hdwy | - | - | 4.13 |  | 6.43 | 6.23 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.43 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.43 | - |
| Follow-up Hdwy | - | - | 2.227 | - | 3.527 | 3.327 |
| Pot Cap-1 Maneuver | - | - | 1332 | - | 663 | 808 |
| Stage 1 | - | - | - | - | 807 | - |
| Stage 2 | - | - | - | - | 921 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1332 | - | 660 | 808 |
| Mov Cap-2 Maneuver | - | - | - | - | 660 | - |
| Stage 1 | - | - | - | - | 807 | - |
| Stage 2 | - | - | - | - | 917 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.4 |  | 9.8 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | WBL WBT |  |
| Capacity (veh/h) |  | 88 | - | - | 1332 | - |
| HCM Lane V/C Ratio |  | . 41 | - | - | 0.004 | - |
| HCM Control Delay (s) |  | 9.8 | - | - | 7.7 | - |
| HCM Lane LOS |  | A | - | - | A | - |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.7 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | -1 | Y |  |
| Traffic Vol, veh/h | 173 | 1 | 2 | 70 | 2 | 15 |
| Future Vol, veh/h | 173 | 1 | 2 | 70 | 2 | 15 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 82 | 82 | 82 | 82 | 82 | 82 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 211 | 1 | 2 | 85 | 2 | 18 |


| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 212 | 0 | 301 | 212 |
| Stage 1 | - | - | - | - | 212 | - |
| Stage 2 | - | - | - | - | 89 | - |
| Critical Hdwy | - | - | 4.13 | - | 6.43 | 6.23 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.43 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.43 | - |
| Follow-up Hdwy | - | - | 2.227 | - | 3.527 | 3.327 |
| Pot Cap-1 Maneuver | - | - | 1352 | - | 688 | 826 |
| Stage 1 | - | - | - | - | 821 | - |
| Stage 2 | - | - | - | - | 932 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1352 | - | 687 | 826 |
| Mov Cap-2 Maneuver | - | - | - | - | 687 | - |
| Stage 1 | - | - | - | - | 821 | - |
| Stage 2 | - | - | - | - | 930 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.2 |  | 9.6 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | WBL WBT |  |
| Capacity (veh/h) |  | 807 | - | - | 1352 | - |
| HCM Lane V/C Ratio |  | 0.026 | - | - | 0.002 | - |
| HCM Control Delay (s) |  | 9.6 | - | - | 7.7 | 0 |
| HCM Lane LOS |  | A | - | - | A | A |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.5 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | 1 |  | 4 |  |
| Traffic Vol, veh/h | 49 | 151 | 44 | 21 | 17 | 21 |
| Future Vol, veh/h | 49 | 151 | 44 | 21 | 17 | 21 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 76 | 76 | 76 | 76 | 76 | 76 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 64 | 199 | 58 | 28 | 22 | 28 |



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | * | 个 4 |  | \% | 㻢 |  | * | $\hat{\sigma}$ |  | \% | $\uparrow$ |  |
| Traffic Volume (veh/h) | 7 | 36 | 2 | 103 | 50 | 400 | 1 | 57 | 123 | 479 | 67 | 13 |
| Future Volume (veh/h) | 7 | 36 | 2 | 103 | 50 | 400 | 1 | 57 | 123 | 479 | 67 | 13 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 0.97 | 1.00 |  | 0.98 | 1.00 |  | 0.98 | 1.00 |  | 0.98 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 |
| Adj Flow Rate, veh/h | 7 | 38 | 2 | 108 | 53 | 421 | 1 | 60 | 129 | 504 | 71 | 14 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, \% | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 16 | 610 | 32 | 136 | 436 | 380 | 2 | 122 | 262 | 548 | 817 | 161 |
| Arrive On Green | 0.01 | 0.18 | 0.18 | 0.08 | 0.25 | 0.25 | 0.00 | 0.24 | 0.24 | 0.31 | 0.54 | 0.54 |
| Sat Flow, veh/h | 1767 | 3403 | 177 | 1767 | 1763 | 1536 | 1767 | 518 | 1113 | 1767 | 1501 | 296 |
| Grp Volume(v), veh/h | 7 | 20 | 20 | 108 | 53 | 421 | 1 | 0 | 189 | 504 | 0 | 85 |
| Grp Sat Flow(s), veh/h/ln | 1767 | 1763 | 1817 | 1767 | 1763 | 1536 | 1767 | 0 | 1631 | 1767 | 0 | 1797 |
| Q Serve(g_s), s | 0.4 | 0.8 | 0.9 | 5.5 | 2.1 | 22.5 | 0.1 | 0.0 | 9.1 | 25.0 | 0.0 | 2.1 |
| Cycle Q Clear(g_c), s | 0.4 | 0.8 | 0.9 | 5.5 | 2.1 | 22.5 | 0.1 | 0.0 | 9.1 | 25.0 | 0.0 | 2.1 |
| Prop In Lane | 1.00 |  | 0.10 | 1.00 |  | 1.00 | 1.00 |  | 0.68 | 1.00 |  | 0.16 |
| Lane Grp Cap(c), veh/h | 16 | 316 | 326 | 136 | 436 | 380 | 2 | 0 | 384 | 548 | 0 | 978 |
| V/C Ratio(X) | 0.44 | 0.06 | 0.06 | 0.79 | 0.12 | 1.11 | 0.41 | 0.00 | 0.49 | 0.92 | 0.00 | 0.09 |
| Avail Cap(c_a), veh/h | 97 | 349 | 360 | 185 | 436 | 380 | 97 | 0 | 384 | 690 | 0 | 978 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 44.8 | 31.0 | 31.0 | 41.2 | 26.5 | 34.2 | 45.4 | 0.0 | 30.0 | 30.3 | 0.0 | 9.9 |
| Incr Delay (d2), s/veh | 18.4 | 0.1 | 0.1 | 15.1 | 0.1 | 78.7 | 85.2 | 0.0 | 4.4 | 15.3 | 0.0 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.2 | 0.4 | 0.4 | 2.9 | 0.9 | 16.3 | 0.1 | 0.0 | 4.0 | 12.6 | 0.0 | 0.8 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 63.2 | 31.1 | 31.1 | 56.4 | 26.7 | 112.9 | 130.6 | 0.0 | 34.5 | 45.5 | 0.0 | 10.1 |
| LnGrp LOS | E | C | C | E | C | F | F | A | C | D | A | B |
| Approach Vol, veh/h |  | 47 |  |  | 582 |  |  | 190 |  |  | 589 |  |
| Approach Delay, s/veh |  | 35.9 |  |  | 94.5 |  |  | 35.0 |  |  | 40.4 |  |
| Approach LOS |  | D |  |  | F |  |  | D |  |  | D |  |


| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), s | 32.7 | 25.9 | 11.5 | 20.8 | 4.6 | 54.0 | 5.3 | 27.0 |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax), s | 35.5 | 19.0 | 9.5 | 18.0 | 5.0 | 49.5 | 5.0 | 22.5 |
| Max Q Clear Time (g_c+11), s | 27.0 | 11.1 | 7.5 | 2.9 | 2.1 | 4.1 | 2.4 | 24.5 |
| Green Ext Time (p_c), s | 1.2 | 0.6 | 0.0 | 0.1 | 0.0 | 0.5 | 0.0 | 0.0 |

Intersection Summary

| HCM 6th Ctrl Delay | 61.9 |
| :--- | ---: |
| HCM 6th LOS | E |

- Opening Year plus Project Conditions



## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 4 | 7 | \% | 4 | 7 | \% | 4 | F | ${ }^{7}$ | 4 | $\stackrel{7}{ }$ |
| Traffic Volume (veh/h) 30 | 272 | 61 | 63 | 114 | 162 | 132 | 168 | 562 | 209 | 88 | 53 |
| Future Volume (veh/h) 30 | 272 | 61 | 63 | 114 | 162 | 132 | 168 | 562 | 209 | 88 | 53 |
| Initial Q $(\mathrm{Qb})$, veh 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) 1.00 |  | 0.98 | 1.00 |  | 0.98 | 0.99 |  | 0.99 | 1.00 |  | 1.00 |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 |
| Adj Flow Rate, veh/h 35 | 316 | 71 | 73 | 133 | 188 | 153 | 195 | 653 | 243 | 102 | 0 |
| Peak Hour Factor 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Percent Heavy Veh, \% 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h 63 | 409 | 341 | 99 | 446 | 370 | 676 | 618 | 605 | 481 | 684 |  |
| Arrive On Green 0.04 | 0.22 | 0.22 | 0.06 | 0.24 | 0.24 | 0.08 | 0.33 | 0.33 | 0.12 | 0.37 | 0.00 |
| Sat Flow, veh/h 1767 | 1856 | 1544 | 1767 | 1856 | 1537 | 1767 | 1856 | 1554 | 1767 | 1856 | 1572 |
| Grp Volume(v), veh/h 35 | 316 | 71 | 73 | 133 | 188 | 153 | 195 | 653 | 243 | 102 | 0 |
| Grp Sat Flow(s),veh/h/ln1767 | 1856 | 1544 | 1767 | 1856 | 1537 | 1767 | 1856 | 1554 | 1767 | 1856 | 1572 |
| Q Serve(g_s), s 1.3 | 10.6 | 2.5 | 2.7 | 3.9 | 7.0 | 3.7 | 5.2 | 22.0 | 5.8 | 2.4 | 0.0 |
| Cycle Q Clear(g_c), s 1.3 | 10.6 | 2.5 | 2.7 | 3.9 | 7.0 | 3.7 | 5.2 | 22.0 | 5.8 | 2.4 | 0.0 |
| Prop In Lane 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h 63 | 409 | 341 | 99 | 446 | 370 | 676 | 618 | 605 | 481 | 684 |  |
| V/C Ratio(X) 0.55 | 0.77 | 0.21 | 0.74 | 0.30 | 0.51 | 0.23 | 0.32 | 1.08 | 0.51 | 0.15 |  |
| Avail Cap(c_a), veh/h 241 | 618 | 514 | 241 | 618 | 512 | 771 | 618 | 605 | 514 | 684 |  |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) $\quad 1.00$ | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh 31.3 | 24.2 | 21.0 | 30.7 | 20.5 | 21.7 | 12.4 | 16.4 | 20.2 | 11.9 | 13.9 | 0.0 |
| Incr Delay (d2), s/veh 7.3 | 3.4 | 0.3 | 10.3 | 0.4 | 1.1 | 0.2 | 1.3 | 59.6 | 0.8 | 0.5 | 0.0 |
| Initial Q Delay(d3),s/veh 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/lm0. 7 | 4.7 | 0.9 | 1.4 | 1.6 | 2.5 | 1.3 | 2.3 | 18.3 | 2.1 | 1.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d), s/veh 38.6 | 27.5 | 21.3 | 41.0 | 20.9 | 22.8 | 12.5 | 17.7 | 79.8 | 12.7 | 14.4 | 0.0 |
| LnGrp LOS D | C | C | D | C | C | B | B | F | B | B |  |
| Approach Vol, veh/h | 422 |  |  | 394 |  |  | 1001 |  |  | 345 | A |
| Approach Delay, s/veh | 27.4 |  |  | 25.5 |  |  | 57.4 |  |  | 13.2 |  |
| Approach LOS | C |  |  | C |  |  | E |  |  | B |  |


| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), $\$ 2.3$ | 26.5 | 8.2 | 19.1 | 9.9 | 28.9 | 6.9 | 20.4 |  |
| Change Period (Y+Rc), s 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |  |
| Max Green Setting (Gmax9.8 | 22.0 | 9.0 | 22.0 | 9.0 | 22.0 | 9.0 | 22.0 |  |
| Max Q Clear Time (g_c+I1才, © | 24.0 | 4.7 | 12.6 | 5.7 | 4.4 | 3.3 | 9.0 |  |
| Green Ext Time (p_c), s | 0.1 | 0.0 | 0.0 | 1.4 | 0.1 | 0.4 | 0.0 | 1.1 |

## Intersection Summary

| HCM 6th Ctrl Delay | 38.7 |
| :--- | ---: |
| HCM 6th LOS | $D$ |

## Notes

Unsignalized Delay for [SBR] is excluded from calculations of the approach delay and intersection delay.


| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | $\uparrow$ | $\stackrel{7}{ }$ |  |  |  |  | 4 | $\underset{ }{7}$ | ${ }^{7}$ | 4 |  |
| Traffic Volume (veh/h) 291 | 1 | 327 | 0 | 0 | 0 | 0 | 571 | 12 | 60 | 151 | 0 |
| Future Volume (veh/h) 291 | 1 | 327 | 0 | 0 | 0 | 0 | 571 | 12 | 60 | 151 | 0 |
| Initial Q $(Q b)$, veh 0 | 0 | 0 |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  |  |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln 1856 | 1856 | 1856 |  |  |  | 0 | 1856 | 1856 | 1856 | 1856 | 0 |
| Adj Flow Rate, veh/h 327 | 1 | 367 |  |  |  | 0 | 642 | 13 | 67 | 170 | 0 |
| Peak Hour Factor 0.89 | 0.89 | 0.89 |  |  |  | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Percent Heavy Veh, \% 3 | 3 | 3 |  |  |  | 0 | 3 | 3 | 3 | 3 | 0 |
| Cap, veh/h 471 | 1 | 421 |  |  |  | 0 | 1016 | 861 | 87 | 1187 | 0 |
| Arrive On Green 0.27 | 0.27 | 0.27 |  |  |  | 0.00 | 0.55 | 0.55 | 0.05 | 0.64 | 0.00 |
| Sat Flow, veh/h 1762 | 5 | 1572 |  |  |  | 0 | 1856 | 1572 | 1767 | 1856 | 0 |
| Grp Volume(v), veh/h 328 | 0 | 367 |  |  |  | 0 | 642 | 13 | 67 | 170 | 0 |
| Grp Sat Flow(s),veh/h/ln1767 | 0 | 1572 |  |  |  | 0 | 1856 | 1572 | 1767 | 1856 | 0 |
| Q Serve(g_s), s 18.4 | 0.0 | 24.5 |  |  |  | 0.0 | 26.3 | 0.4 | 4.1 | 4.0 | 0.0 |
| Cycle Q Clear(g_c), s 18.4 | 0.0 | 24.5 |  |  |  | 0.0 | 26.3 | 0.4 | 4.1 | 4.0 | 0.0 |
| Prop In Lane 1.00 |  | 1.00 |  |  |  | 0.00 |  | 1.00 | 1.00 |  | 0.00 |
| Lane Grp Cap(c), veh/h 473 | 0 | 421 |  |  |  | 0 | 1016 | 861 | 87 | 1187 | 0 |
| V/C Ratio(X) 0.69 | 0.00 | 0.87 |  |  |  | 0.00 | 0.63 | 0.02 | 0.77 | 0.14 | 0.00 |
| Avail Cap(c_a), veh/h 641 | 0 | 570 |  |  |  | 0 | 1016 | 861 | 326 | 1187 | 0 |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) 1.00 | 0.00 | 1.00 |  |  |  | 0.00 | 1.00 | 1.00 | 0.98 | 0.98 | 0.00 |
| Uniform Delay (d), s/veh 36.2 | 0.0 | 38.5 |  |  |  | 0.0 | 17.2 | 11.3 | 51.7 | 7.9 | 0.0 |
| Incr Delay (d2), s/veh 2.0 | 0.0 | 10.8 |  |  |  | 0.0 | 3.0 | 0.0 | 13.0 | 0.2 | 0.0 |
| Initial Q Delay(d3),s/veh 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln8.1 | 0.0 | 10.6 |  |  |  | 0.0 | 11.6 | 0.2 | 2.1 | 1.6 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh 38.2 | 0.0 | 49.3 |  |  |  | 0.0 | 20.2 | 11.4 | 64.6 | 8.1 | 0.0 |
| LnGrp LOS D | A | D |  |  |  | A | C | B | E | A | A |
| Approach Vol, veh/h | 695 |  |  |  |  |  | 655 |  |  | 237 |  |
| Approach Delay, s/veh | 44.1 |  |  |  |  |  | 20.0 |  |  | 24.1 |  |
| Approach LOS | D |  |  |  |  |  | C |  |  | C |  |


| Timer - Assigned Phs | 1 | 2 | 4 | 6 |
| :--- | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), $\$ 0.1$ | 65.3 | 34.5 | 75.5 |  |
| Change Period (Y+Rc), s* 4.7 | 5.1 | 5.1 | 5.1 |  |
| Max Green Setting (Gmax) 28 | 34.9 | 39.9 | 34.9 |  |
| Max Q Clear Time (g_c+110, s | 28.3 | 26.5 | 6.0 |  |
| Green Ext Time (p_c), s | 0.1 | 2.4 | 2.9 | 1.0 |

Intersection Summary

| HCM 6th Ctrl Delay | 31.2 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Intersection |
| :--- |
| Intersection Delay, s/veh18.9 |
| Intersection LOS $\quad$ C |


| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Configurations | M |  |  | $\uparrow$ | 4 | $\mathbf{~}$ |
| Traffic Vol, veh/h | 266 | 20 | 6 | 340 | 351 | 114 |
| Future Vol, veh/h | 266 | 20 | 6 | 340 | 351 | 114 |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 302 | 23 | 7 | 386 | 399 | 130 |
| Number of Lanes | 1 | 0 | 0 | 1 | 2 | 1 |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| Opposing Approach |  | SB | NB |
| Opposing Lanes | 0 | 3 | 1 |
| Conflicting Approach Left SB | EB |  |  |
| Conflicting Lanes Left | 3 | 1 | 0 |
| Conflicting Approach RighNB |  | EB |  |
| Conflicting Lanes Right | 1 | 0 | 1 |
| HCM Control Delay | 23.4 | 24.8 | 11.7 |
| HCM LOS | C | C | B |


| Lane | NBLn1 EBLn1 SBLn1 SBLn2 SBLn3 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $2 \%$ | $93 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $98 \%$ | $0 \%$ | $100 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, \% | $0 \%$ | $7 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 346 | 286 | 176 | 176 | 114 |
| LT Vol | 6 | 266 | 0 | 0 | 0 |
| Through Vol | 340 | 0 | 176 | 176 | 0 |
| RT Vol | 0 | 20 | 0 | 0 | 114 |
| Lane Flow Rate | 393 | 325 | 199 | 199 | 130 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.721 | 0.661 | 0.361 | 0.361 | 0.144 |
| Departure Headway (Hd) | 6.603 | 7.323 | 6.508 | 6.508 | 4.006 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 543 | 491 | 548 | 548 | 881 |
| Service Time | 4.392 | 5.1 | 4.299 | 4.299 | 1.795 |
| HCM Lane V/C Ratio | 0.724 | 0.662 | 0.363 | 0.363 | 0.148 |
| HCM Control Delay | 24.8 | 23.4 | 13 | 13 | 7.5 |
| HCM Lane LOS | C | C | B | B | A |
| HCM 95th-tile Q | 5.9 | 4.8 | 1.6 | 1.6 | 0.5 |


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh 13 |  |
| Intersection LOS | B |



| Lane | NBLn1 WBLn1 WBLn2 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $100 \%$ | $0 \%$ | $47 \%$ |
| Vol Thru, \% | $84 \%$ | $0 \%$ | $0 \%$ | $53 \%$ |
| Vol Right, \% | $16 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 37 | 8 | 319 | 363 |
| LT Vol | 0 | 8 | 0 | 169 |
| Through Vol | 31 | 0 | 0 | 194 |
| RT Vol | 6 | 0 | 319 | 0 |
| Lane Flow Rate | 41 | 9 | 351 | 399 |
| Geometry Grp | 2 | 7 | 7 | 2 |
| Degree of Util (X) | 0.061 | 0.015 | 0.482 | 0.553 |
| Departure Headway (Hd) | 5.39 | 6.165 | 4.954 | 4.991 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 668 | 577 | 722 | 718 |
| Service Time | 3.39 | 3.938 | 2.727 | 3.063 |
| HCM Lane V/C Ratio | 0.061 | 0.016 | 0.486 | 0.556 |
| HCM Control Delay | 8.7 | 9 | 12.3 | 14.1 |
| HCM Lane LOS | A | A | B | B |
| HCM 95th-tile Q | 0.2 | 0 | 2.6 | 3.4 |



| Major/Minor | Major1 | Major2 |  |  | Minor1 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Conflicting Flow All | 0 | 0 | 51 | 0 | 354 | 47 |  |
| $\quad$ Stage 1 | - | - | - | - | 47 | - |  |
| Stage 2 | - | - | - | - | 307 | - |  |
| Critical Hdwy | - | - | 4.13 | - | 6.43 | 6.23 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.43 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.43 | - |  |
| Follow-up Hdwy | - | - | 2.227 | - | 3.527 | 3.327 |  |
| Pot Cap-1 Maneuver | - | - | 1549 | - | 642 | 1019 |  |
| Stage 1 | - | - | - | - | 973 | - |  |
| Stage 2 | - | - | - | - | 744 | - |  |
| Platoon blocked, \% | - | - |  | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | 1549 | - | 629 | 1019 |  |
| Mov Cap-2 Maneuver | - | - | - | - | 629 | - |  |
| Stage 1 | - | - | - | - | 973 | - |  |
| Stage 2 | - | - | - | - | 728 | - |  |


| Approach | EB | WB | NB |
| :--- | ---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.9 | 9.7 |

HCMLOS A


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.2 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\hat{\imath}$ |  |  | - | r |  |
| Traffic Vol, veh/h | 27 | 53 | 36 | 156 | 2 | 6 |
| Future Vol, veh/h | 27 | 53 | 36 | 156 | 2 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 61 | 61 | 61 | 61 | 61 | 61 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 44 | 87 | 59 | 256 | 3 | 10 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.3 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | -1 | 1 |  | 4 |  |
| Traffic Vol, veh/h | 13 | 64 | 142 | 5 | 13 | 43 |
| Future Vol, veh/h | 13 | 64 | 142 | 5 | 13 | 43 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 88 | 88 | 88 | 88 | 88 | 88 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 15 | 73 | 161 | 6 | 15 | 49 |


| Major/Minor | Major1 | Major2 |  |  | Minor2 |  |  |
| :--- | ---: | :--- | :--- | :--- | :--- | ---: | :---: |
| Conflicting Flow All | 167 | 0 | - | 0 | 267 | 164 |  |
| Stage 1 | - | - | - | - | 164 | - |  |
| Stage 2 | - | - | - | - | 103 | - |  |
| Critical Hdwy | 4.13 | - | - | - | 6.43 | 6.23 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.43 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.43 | - |  |
| Follow-up Hdwy | 2.227 | - | - | -3.527 | 3.327 |  |  |
| Pot Cap-1 Maneuver | 1405 | - | - | - | 720 | 878 |  |
| $\quad$ Stage 1 | - | - | - | - | 863 | - |  |
| Stage 2 | - | - | - | - | 919 | - |  |
| Platoon blocked, \% |  | - | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1405 | - | - | - | 712 | 878 |  |
| Mov Cap-2 Maneuver | - | - | - | - | 712 | - |  |
| Stage 1 | - | - | - | - | 854 | - |  |
| Stage 2 | - | - | - | - | 919 | - |  |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 1.3 | 0 | 9.7 |

HCMLOS A

| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1405 | - | - | -833 |
| HCM Lane V/C Ratio | 0.011 | - | - | -0.076 |
| HCM Control Delay (s) | 7.6 | 0 | - | - |
| HCM Lane LOS | A | A | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | - | - |
| HC | 0.2 |  |  |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{4}$ | 个食 |  | \% | $\uparrow$ |  | \% | $\dagger$ |  | \% | $\hat{\beta}$ |  |
| Traffic Volume (veh/h) | 33 | 50 | 2 | 89 | 24 | 555 | 0 | 74 | 102 | 472 | 61 | 21 |
| Future Volume (veh/h) | 33 | 50 | 2 | 89 | 24 | 555 | 0 | 74 | 102 | 472 | 61 | 21 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 0.99 | 1.00 |  | 0.99 | 1.00 |  | 0.97 | 1.00 |  | 0.98 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 |
| Adj Flow Rate, veh/h | 41 | 62 | 2 | 110 | 30 | 685 | 0 | 91 | 126 | 583 | 75 | 26 |
| Peak Hour Factor | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 |
| Percent Heavy Veh, \% | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 59 | 910 | 29 | 139 | 540 | 477 | 2 | 212 | 294 | 321 | 695 | 241 |
| Arrive On Green | 0.03 | 0.26 | 0.26 | 0.08 | 0.31 | 0.31 | 0.00 | 0.31 | 0.31 | 0.18 | 0.53 | 0.53 |
| Sat Flow, veh/h | 1767 | 3485 | 112 | 1767 | 1763 | 1557 | 1767 | 693 | 960 | 1767 | 1309 | 454 |
| Grp Volume(v), veh/h | 41 | 31 | 33 | 110 | 30 | 685 | 0 | 0 | 217 | 583 | 0 | 101 |
| Grp Sat Flow(s),veh/h/n | 1767 | 1763 | 1834 | 1767 | 1763 | 1557 | 1767 | 0 | 1653 | 1767 | 0 | 1762 |
| Q Serve(g_s), s | 2.4 | 1.4 | 1.4 | 6.4 | 1.3 | 32.0 | 0.0 | 0.0 | 11.0 | 19.0 | 0.0 | 3.0 |
| Cycle Q Clear(g_c), s | 2.4 | 1.4 | 1.4 | 6.4 | 1.3 | 32.0 | 0.0 | 0.0 | 11.0 | 19.0 | 0.0 | 3.0 |
| Prop In Lane | 1.00 |  | 0.06 | 1.00 |  | 1.00 | 1.00 |  | 0.58 | 1.00 |  | 0.26 |
| Lane Grp Cap(c), veh/h | 59 | 460 | 479 | 139 | 540 | 477 | 2 | 0 | 506 | 321 | 0 | 936 |
| V/C Ratio(X) | 0.70 | 0.07 | 0.07 | 0.79 | 0.06 | 1.44 | 0.00 | 0.00 | 0.43 | 1.81 | 0.00 | 0.11 |
| Avail Cap(c_a), veh/h | 321 | 540 | 562 | 321 | 540 | 477 | 321 | 0 | 506 | 321 | 0 | 936 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 50.0 | 29.0 | 29.0 | 47.3 | 25.6 | 36.2 | 0.0 | 0.0 | 28.9 | 42.7 | 0.0 | 12.2 |
| Incr Delay (d2), s/veh | 13.8 | 0.1 | 0.1 | 9.7 | 0.0 | 208.1 | 0.0 | 0.0 | 2.6 | 378.4 | 0.0 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.3 | 0.6 | 0.6 | 3.1 | 0.5 | 39.3 | 0.0 | 0.0 | 4.7 | 42.0 | 0.0 | 1.2 |

Unsig. Movement Delay, s/veh

| LnGrp Delay(d), s/veh | 63.8 | 29.1 | 29.1 | 57.0 | 25.6 | 244.3 | 0.0 | 0.0 | 31.6 | 421.2 | 0.0 | 12.4 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LnGrp LOS | E | C | C | E | C | F | A | A | C | F | A | B |
| Approach Vol, veh/h |  | 105 |  |  | 825 |  |  | 217 |  | 684 |  |  |
| Approach Delay, s/veh |  | 42.6 |  |  | 211.4 |  |  | 31.6 |  | 360.8 |  |  |
| Approach LOS | D |  |  | F |  |  | C |  | F |  |  |  |


| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), s | 23.5 | 36.5 | 12.7 | 31.8 | 0.0 | 60.0 | 8.0 | 36.5 |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax), s | 19.0 | 32.0 | 19.0 | 32.0 | 19.0 | 32.0 | 19.0 | 32.0 |
| Max Q Clear Time (g_c+I1), s | 21.0 | 13.0 | 8.4 | 3.4 | 0.0 | 5.0 | 4.4 | 34.0 |
| Green Ext Time (p_c), s | 0.0 | 1.2 | 0.2 | 0.3 | 0.0 | 0.5 | 0.1 | 0.0 |

Intersection Summary

| HCM 6th Ctrl Delay | 236.2 |
| :--- | ---: |
| HCM 6th LOS | F |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.4 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | r |  |  | - | 个 |  |
| Traffic Vol, veh/h | 0 | 0 | 4 | 0 | 0 | 70 |
| Future Vol, veh/h | 0 | 0 | 4 | 0 | 0 | 70 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, $\#$ | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 0 | 0 | 4 | 0 | 0 | 76 |


| Major/Minor M | Minor2 |  | Major1 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 46 | 38 | 76 | 0 | - | 0 |
| Stage 1 | 38 | - | - | - | - | - |
| Stage 2 | 8 | - | - | - | - | - |
| Critical Hdwy | 6.43 | 6.23 | 4.13 | - | - | - |
| Critical Hdwy Stg 1 | 5.43 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.43 | - | - | - | - | - |
| Follow-up Hdwy | 3.527 | 3.327 | 2.227 | - | - | - |
| Pot Cap-1 Maneuver | 962 | 1031 | 1517 | - | - | - |
| Stage 1 | 982 | - | - | - | - | - |
| Stage 2 | 1012 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 959 | 1031 | 1517 | - | - | - |
| Mov Cap-2 Maneuver | 959 | - | - | - | - | - |
| Stage 1 | 979 | - | - | - | - | - |
| Stage 2 | 1012 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | NB |  | SB |  |
| HCM Control Delay, s | 0 |  | 7.4 |  | 0 |  |
| HCM LOS | A |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBL NBT EBLn1 |  |  | 1 SBT |  |
| Capacity (veh/h) |  | 1517 | - | - | - | - |
| HCM Lane V/C Ratio |  | 0.003 | - | - | - | - |
| HCM Control Delay (s) |  | 7.4 | 0 | 0 | - | - |
| HCM Lane LOS |  | A | A | A | - | - |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | - |



## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 4 | 「 | ${ }^{*}$ | 4 | I' | * | 4 | 「 | ${ }^{*}$ | 4 | $\stackrel{1}{1}$ |
| Traffic Volume (veh/h) 27 | 180 | 112 | 161 | 103 | 156 | 153 | 238 | 824 | 219 | 213 | 58 |
| Future Volume (veh/h) 27 | 180 | 112 | 161 | 103 | 156 | 153 | 238 | 824 | 219 | 213 | 58 |
| Initial Q $(Q b)$, veh 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) 1.00 |  | 0.94 | 1.00 |  | 0.97 | 0.99 |  | 0.96 | 1.00 |  | 1.00 |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 |
| Adj Flow Rate, veh/h 28 | 188 | 117 | 168 | 107 | 162 | 159 | 248 | 858 | 228 | 222 | 0 |
| Peak Hour Factor 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh, \% 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h 52 | 311 | 249 | 214 | 481 | 394 | 593 | 685 | 747 | 421 | 737 |  |
| Arrive On Green 0.03 | 0.17 | 0.17 | 0.12 | 0.26 | 0.26 | 0.08 | 0.37 | 0.37 | 0.11 | 0.40 | 0.00 |
| Sat Flow, veh/h 1767 | 1856 | 1483 | 1767 | 1856 | 1518 | 1767 | 1856 | 1508 | 1767 | 1856 | 1572 |
| Grp Volume(v), veh/h 28 | 188 | 117 | 168 | 107 | 162 | 159 | 248 | 858 | 228 | 222 | 0 |
| Grp Sat Flow(s),veh/h/ln1767 | 1856 | 1483 | 1767 | 1856 | 1518 | 1767 | 1856 | 1508 | 1767 | 1856 | 1572 |
| Q Serve(g_s), s $\quad 1.2$ | 7.2 | 5.5 | 7.1 | 3.5 | 6.8 | 4.2 | 7.5 | 28.4 | 6.0 | 6.3 | 0.0 |
| Cycle Q Clear(g_c), s 1.2 | 7.2 | 5.5 | 7.1 | 3.5 | 6.8 | 4.2 | 7.5 | 28.4 | 6.0 | 6.3 | 0.0 |
| Prop In Lane 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h 52 | 311 | 249 | 214 | 481 | 394 | 593 | 685 | 747 | 421 | 737 |  |
| V/C Ratio(X) 0.54 | 0.60 | 0.47 | 0.78 | 0.22 | 0.41 | 0.27 | 0.36 | 1.15 | 0.54 | 0.30 |  |
| Avail Cap(c_a), veh/h 140 | 471 | 377 | 955 | 1326 | 1086 | 694 | 685 | 747 | 587 | 737 |  |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh 36.8 | 29.6 | 28.9 | 32.8 | 22.3 | 23.6 | 12.9 | 17.6 | 19.7 | 12.7 | 15.9 | 0.0 |
| Incr Delay (d2), s/veh 8.5 | 1.9 | 1.4 | 6.2 | 0.2 | 0.7 | 0.2 | 1.5 | 81.9 | 1.1 | 1.0 | 0.0 |
| Initial Q Delay(d3), s/veh 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/lm0. 6 | 3.3 | 2.0 | 3.3 | 1.5 | 2.4 | 1.6 | 3.3 | 28.8 | 2.3 | 2.7 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh 45.3 | 31.5 | 30.3 | 39.0 | 22.6 | 24.3 | 13.2 | 19.1 | 101.6 | 13.8 | 16.9 | 0.0 |
| LnGrp LOS D | C | C | D | C | C | B | B | F | B | B |  |
| Approach Vol, veh/h | 333 |  |  | 437 |  |  | 1265 |  |  | 450 | A |
| Approach Delay, s/veh | 32.2 |  |  | 29.5 |  |  | 74.3 |  |  | 15.3 |  |
| Approach LOS | C |  |  | C |  |  | E |  |  | B |  |


| Timer - Assigned Phs | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), $\$ 2.8$ | 32.9 | 13.8 | 17.4 | 10.6 | 35.0 | 6.7 | 24.4 |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax.5.5 | 25.5 | 41.5 | 19.5 | 10.5 | 30.5 | 6.1 | 54.9 |
| Max Q Clear Time (g_c +18, , s | 30.4 | 9.1 | 9.2 | 6.2 | 8.3 | 3.2 | 8.8 |
| Green Ext Time (p_c), s 0.4 | 0.0 | 0.5 | 1.0 | 0.2 | 1.2 | 0.0 | 2 |

Intersection Summary

| HCM 6th Ctrl Delay | 50.1 |
| :--- | ---: |
| HCM 6th LOS | D |

## Notes

Unsignalized Delay for [SBR] is excluded from calculations of the approach delay and intersection delay.



## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.


| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Configurations | $\boldsymbol{M}$ |  |  | $\uparrow$ | $\boldsymbol{\uparrow} \uparrow$ | $\mathbf{~}$ |
| Traffic Vol, veh/h | 168 | 19 | 16 | 549 | 502 | 260 |
| Future Vol, veh/h | 168 | 19 | 16 | 549 | 502 | 260 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles, $\%$ | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 177 | 20 | 17 | 578 | 528 | 274 |
| Number of Lanes | 1 | 0 | 0 | 1 | 2 | 1 |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| Opposing Approach |  |  | SB |
| Opposing Lanes | 0 | 3 | NB |
| Conflicting Approach Left SB | SB | 1 |  |
| Conflicting Lanes Left | 3 | 1 | 0 |
| Conflicting Approach RighNB |  | EB |  |
| Conflicting Lanes Right | 1 | 0 | 1 |
| HCM Control Delay | 16.8 | 76.1 | 12 |
| HCM LOS | C | F | B |


| Lane | NBLn1 EBLn1 SBLn1 SBLn2 SBLn3 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $3 \%$ | $\%$ |  | $00 \%$ | $0 \%$ |
| Vol Thru, \% | $97 \%$ | $0 \%$ | $100 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, \% | $0 \%$ | $10 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 565 | 187 | 251 | 251 | 260 |
| LT Vol | 16 | 168 | 0 | 0 | 0 |
| Through Vol | 549 | 0 | 251 | 251 | 0 |
| RT Vol | 0 | 19 | 0 | 0 | 260 |
| Lane Flow Rate | 595 | 197 | 264 | 264 | 274 |
| Geometry Grp | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 1.049 | 0.43 | 0.451 | 0.451 | 0.281 |
| Departure Headway (Hd) | 6.347 | 8.097 | 6.298 | 6.298 | 3.799 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 571 | 447 | 576 | 576 | 952 |
| Service Time | 4.089 | 5.797 | 3.998 | 3.998 | 1.499 |
| HCM Lane V/C Ratio | 1.042 | 0.441 | 0.458 | 0.458 | 0.288 |
| HCM Control Delay | 76.1 | 16.8 | 14.1 | 14.1 | 8 |
| HCM Lane LOS | F | C | B | B | A |
| HCM 95th-tile Q | 16.7 | 2.1 | 2.3 | 2.3 | 1.2 |

Intersection
Intersection Delay, s/veh23.5
Intersection LOS $\quad$ C

| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Configurations | 16 | $\mathbf{r}$ | $\hat{f}$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 16 | 350 | 217 | 18 | 468 | 50 |
| Future Vol, veh/h | 16 | 350 | 217 | 18 | 468 | 50 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 16 | 361 | 224 | 19 | 482 | 52 |
| Number of Lanes | 1 | 1 | 1 | 0 | 0 | 1 |
| Approach | WB |  | NB |  | SB |  |
| Opposing Approach |  |  | SB | NB |  |  |
| Opposing Lanes | 0 | 1 | 1 |  |  |  |
| Conflicting Approach Left NB |  |  | WB |  |  |  |
| Conflicting Lanes Left | 1 | 0 | 2 |  |  |  |
| Conflicting Approach RighISB | WB |  |  |  |  |  |
| Conflicting Lanes Right | 1 | 2 | 0 |  |  |  |
| HCM Control Delay | 17.1 | 13 | 32.7 |  |  |  |
| HCM LOS | C | B | D |  |  |  |


| Lane | NBLn1WBLn1WBLn2 SBLn1 |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $100 \%$ | $0 \%$ | $90 \%$ |
| Vol Thru, \% | $92 \%$ | $0 \%$ | $0 \%$ | $10 \%$ |
| Vol Right, $\%$ | $8 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 235 | 16 | 350 | 518 |
| LT Vol | 0 | 16 | 0 | 468 |
| Through Vol | 217 | 0 | 0 | 50 |
| RT Vol | 18 | 0 | 350 | 0 |
| Lane Flow Rate | 242 | 16 | 361 | 534 |
| Geometry Grp | 2 | 7 | 7 | 2 |
| Degree of Util (X) | 0.401 | 0.033 | 0.6 | 0.848 |
| Departure Headway (Hd) | 5.965 | 7.21 | 5.988 | 5.715 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 598 | 495 | 599 | 630 |
| Service Time | 4.041 | 4.98 | 3.757 | 3.775 |
| HCM Lane V/C Ratio | 0.405 | 0.032 | 0.603 | 0.848 |
| HCM Control Delay | 13 | 10.2 | 17.4 | 32.7 |
| HCM Lane LOS | B | B | C | D |
| HCM 95th-tile Q | 1.9 | 0.1 | 4 | 9.4 |



| Major/Minor | Major1 | Major2 | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0253 | 0353 | 252 |
| Stage 1 | - | - - | 252 | - |
| Stage 2 | - | - - | 101 |  |
| Critical Hdwy | - | 4.13 | 6.43 | 6.23 |
| Critical Hdwy Stg 1 | - | - - | - 5.43 | - |
| Critical Hdwy Stg 2 | - | - - | - 5.43 | - |
| Follow-up Hdwy | - | - 2.227 | - 3.527 | 3.327 |
| Pot Cap-1 Maneuver | - | 1306 | 643 | 784 |
| Stage 1 | - | - - | 788 | - |
| Stage 2 | - | - - | - 921 | - |
| Platoon blocked, \% | - | - | - |  |
| Mov Cap-1 Maneuver | - | 1306 | - 640 | 784 |
| Mov Cap-2 Maneuver | - | - | - 640 | - |
| Stage 1 | - | - - | - 788 | - |
| Stage 2 | - | - - | - 917 | - |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, $s$ | 0 | 0.4 | 9.9 |

HCMLOS A


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.9 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\hat{7}$ |  |  | $\uparrow$ | 1 |  |
| Traffic Vol, veh/h | 173 | 1 | 2 | 70 | 55 | 33 |
| Future Vol, veh/h | 173 | 1 | 2 | 70 | 55 | 33 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 82 | 82 | 82 | 82 | 82 | 82 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 211 | 1 | 2 | 85 | 67 | 40 |


| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 212 | 0 | 301 | 212 |
| Stage 1 | - | - | - | - | 212 | - |
| Stage 2 | - | - | - | - | 89 | - |
| Critical Hdwy | - | - | 4.13 | - | 6.43 | 6.23 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.43 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.43 | - |
| Follow-up Hdwy | - | - | 2.227 | - | 3.527 | 3.327 |
| Pot Cap-1 Maneuver | - | - | 1352 | - | 688 | 826 |
| Stage 1 | - | - | - | - | 821 | - |
| Stage 2 | - | - | - | - | 932 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1352 | - | 687 | 826 |
| Mov Cap-2 Maneuver | - | - | - | - | 687 | - |
| Stage 1 | - | - | - | - | 821 | - |
| Stage 2 | - | - | - | - | 930 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.2 |  | 10.8 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | WBL WBT |  |
| Capacity (veh/h) |  | 733 | - | - | 1352 | - |
| HCM Lane V/C Ratio |  | 0.146 | - | - | 0.002 | - |
| HCM Control Delay (s) |  | 10.8 | - | - | 7.7 | 0 |
| HCM Lane LOS |  | B | - | - | A | A |
| HCM 95th \%tile Q(veh) |  | 0.5 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.2 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | -1 | 1 |  | 4 |  |
| Traffic Vol, veh/h | 49 | 151 | 90 | 28 | 17 | 21 |
| Future Vol, veh/h | 49 | 151 | 90 | 28 | 17 | 21 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 76 | 76 | 76 | 76 | 76 | 76 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 64 | 199 | 118 | 37 | 22 | 28 |


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 155 | 0 | - - | 0 | 464 | 137 |
| Stage 1 | - | - | - - | - | 137 | - |
| Stage 2 | - | - | - - | - | 327 | - |
| Critical Hdwy | 4.13 | - | - - | - | 6.43 | 6.23 |
| Critical Hdwy Stg 1 | - | - | - - | - | 5.43 | - |
| Critical Hdwy Stg 2 | - | - | - - | - | 5.43 | - |
| Follow-up Hdwy | 2.227 | - | - - | - | 3.527 | 3.327 |
| Pot Cap-1 Maneuver | 1419 | - | - - | - | 555 | 909 |
| Stage 1 | - | - | - - | - | 887 | - |
| Stage 2 | - | - | - - | - | 728 | - |
| Platoon blocked, \% |  | - | - - | - |  |  |
| Mov Cap-1 Maneuver | 1419 | - | - - | - | 527 | 909 |
| Mov Cap-2 Maneuver | - | - | - - | - | 527 | - |
| Stage 1 | - | - | - - | - | 842 | - |
| Stage 2 | - | - | - - | - | 728 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 1.9 |  | 0 |  | 10.7 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1419 | - | - | - | 686 |
| HCM Lane V/C Ratio |  | 0.045 |  | - | - | 0.073 |
| HCM Control Delay (s) |  | 7.7 | 0 | - | - | 10.7 |
| HCM Lane LOS |  | A | A A | - | - | B |
| HCM 95th \%tile Q(veh) |  | 0.1 | A | - | - | 0.2 |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 个 ${ }^{\text {P }}$ |  | \% |  |  | ${ }^{7}$ | $\hat{\dagger}$ |  | K | $\uparrow$ |  |
| Traffic Volume (veh/h) | 7 | 36 | 2 | 103 | 50 | 400 | 1 | 58 | 128 | 479 | 67 | 13 |
| Future Volume (veh/h) | 7 | 36 | 2 | 103 | 50 | 400 | 1 | 58 | 128 | 479 | 67 | 13 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 0.97 | 1.00 |  | 0.98 | 1.00 |  | 0.98 | 1.00 |  | 0.98 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 | 1856 |
| Adj Flow Rate, veh/h | 7 | 38 | 2 | 108 | 53 | 421 | 1 | 61 | 135 | 504 | 71 | 14 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, \% | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 16 | 610 | 32 | 136 | 436 | 380 | 2 | 119 | 264 | 548 | 817 | 161 |
| Arrive On Green | 0.01 | 0.18 | 0.18 | 0.08 | 0.25 | 0.25 | 0.00 | 0.24 | 0.24 | 0.31 | 0.54 | 0.54 |
| Sat Flow, veh/h | 1767 | 3403 | 177 | 1767 | 1763 | 1536 | 1767 | 507 | 1122 | 1767 | 1501 | 296 |
| Grp Volume(v), veh/h | 7 | 20 | 20 | 108 | 53 | 421 | 1 | 0 | 196 | 504 | 0 | 85 |
| Grp Sat Flow(s),veh/h/ln | 1767 | 1763 | 1817 | 1767 | 1763 | 1536 | 1767 | 0 | 1629 | 1767 | 0 | 1797 |
| Q Serve(g_s), s | 0.4 | 0.8 | 0.9 | 5.5 | 2.1 | 22.5 | 0.1 | 0.0 | 9.5 | 25.0 | 0.0 | 2.1 |
| Cycle Q Clear(g_c), s | 0.4 | 0.8 | 0.9 | 5.5 | 2.1 | 22.5 | 0.1 | 0.0 | 9.5 | 25.0 | 0.0 | 2.1 |
| Prop In Lane | 1.00 |  | 0.10 | 1.00 |  | 1.00 | 1.00 |  | 0.69 | 1.00 |  | 0.16 |
| Lane Grp Cap(c), veh/h | 16 | 316 | 326 | 136 | 436 | 380 | 2 | 0 | 384 | 548 | 0 | 978 |
| V/C Ratio(X) | 0.44 | 0.06 | 0.06 | 0.79 | 0.12 | 1.11 | 0.41 | 0.00 | 0.51 | 0.92 | 0.00 | 0.09 |
| Avail Cap(c_a), veh/h | 97 | 349 | 360 | 185 | 436 | 380 | 97 | 0 | 384 | 690 | 0 | 978 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 44.8 | 31.0 | 31.0 | 41.2 | 26.5 | 34.2 | 45.4 | 0.0 | 30.2 | 30.3 | 0.0 | 9.9 |
| Incr Delay (d2), s/veh | 18.4 | 0.1 | 0.1 | 15.1 | 0.1 | 78.7 | 85.2 | 0.0 | 4.8 | 15.3 | 0.0 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/In | 0.2 | 0.4 | 0.4 | 2.9 | 0.9 | 16.3 | 0.1 | 0.0 | 4.2 | 12.6 | 0.0 | 0.8 |

Unsig. Movement Delay, s/veh

| LnGrp Delay(d), s/veh | 63.2 | 31.1 | 31.1 | 56.4 | 26.7 | 112.9 | 130.6 | 0.0 | 35.0 | 45.5 | 0.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LnGrp LOS | E | C | C | E | C | F | F | A | C | D | A |
| Approach Vol, veh/h |  | 47 |  |  | 582 |  | 197 |  | B |  |  |
| Approach Delay, s/veh |  | 35.9 |  |  | 94.5 |  |  | 35.5 |  | 409 |  |
| Approach LOS | D |  |  | F |  |  | D |  | D |  |  |


| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), s | 32.7 | 25.9 | 11.5 | 20.8 | 4.6 | 54.0 | 5.3 | 27.0 |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax), s | 35.5 | 19.0 | 9.5 | 18.0 | 5.0 | 49.5 | 5.0 | 22.5 |
| Max Q Clear Time (g_c+I1), s | 27.0 | 11.5 | 7.5 | 2.9 | 2.1 | 4.1 | 2.4 | 24.5 |
| Green Ext Time (p_c), s | 1.2 | 0.6 | 0.0 | 0.1 | 0.0 | 0.5 | 0.0 | 0.0 |

Intersection Summary

| HCM 6th Ctrl Delay | 61.8 |
| :--- | ---: |
| HCM 6th LOS | E |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 8.7 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | r |  |  | - | 个 |  |
| Traffic Vol, veh/h | 70 | 4 | 0 | 0 | 0 | 0 |
| Future Vol, veh/h | 70 | 4 | 0 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 96 | 96 | 96 | 96 | 96 | 96 |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 |
| Mvmt Flow | 73 | 4 | 0 | 0 | 0 | 0 |


| Major/Minor | Minor2 | Major1 |  | Major2 |  |  |
| :--- | ---: | ---: | ---: | :--- | :--- | :--- |
| Conflicting Flow All | 1 | 1 | 1 | 0 | - | 0 |
| $\quad$ Stage 1 | 1 | - | - | - | - | - |
| $\quad$ Stage 2 | 0 | - | - | - | - | - |
| Critical Hdwy | 6.43 | 6.23 | 4.13 | - | - | - |
| Critical Hdwy Stg 1 | 5.43 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.43 | - | - | - | - | - |
| Follow-up Hdwy | 3.527 | 3.327 | 2.227 | - | - | - |
| Pot Cap-1 Maneuver | 1019 | 1081 | 1615 | - | - | - |
| $\quad$ Stage 1 | 1020 | - | - | - | - | - |
| $\quad$ Stage 2 | - | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 1019 | 1081 | 1615 | - | - | - |
| Mov Cap-2 Maneuver | 1019 | - | - | - | - | - |
| Stage 1 | 1020 | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
|  |  |  |  |  |  |  |


| Approach | EB | NB | SB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 8.8 | 0 | 0 |

HCMLOS A

| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |
| :--- | ---: | ---: | ---: | :---: |
| Capacity (veh/h) | 1615 | -1022 | - | - |
| HCM Lane V/C Ratio | - | -0.075 | - | - |
| HCM Control Delay (s) | 0 | - | 8.8 | - |
| HCM Lane LOS | A | - | A | - |
| HCM 95th \%tile Q(veh) | 0 | - | 0.2 | - |


[^0]:    Notes: PCE - Passenger Car Equivalent

[^1]:    Notes: AWSC - All way stop control

